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2 CHAPTER TWO: ELECTRICAL RELAXATION

3 1/29/2018

4 [FINAL DRAFT]

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65			

66

## 67 Preliminaries

68 The examples used to illustrate different applications are not central to the purpose of this  
69 book and are not recent. Some of the applications have been discussed in an unpublished but  
70 widely circulated paper by the present author that is reproduced in Appendix A (original errors  
71 have been corrected and the conversion to the phase convention used by everyone except  
72 electrical engineers has been made.)

73

## 74 2.1 Nomenclature

75 Italicized lower case letters are used for physical variables, e.g. {x, y, z, r} for distances, t for  
76 time, and q for charge; italicized upper case letters are used for specific values of variables and  
77 field magnitudes, e.g. {X, Y, Z, R}, T, Q. Vectors are denoted by bold face upper case letters with  
78 an arrow  $\vec{\mathbf{V}}$  and tensors are denoted by bold face upper case  $\mathbf{T}$ .

79 There are two time constants for relaxation of polarization, one for relaxation at constant  
80 electric field (i.e. dielectric relaxation of the displacement  $\vec{\mathbf{D}}$ ) denoted by  $\tau_E$  and one for  
81 relaxation at constant displacement (i.e. conductivity relaxation of the electric field  $\vec{\mathbf{E}}$ ) denoted  
82 by  $\tau_D$ . Amongst other things these two distinct time constants correspond to two microscopic  
83 time constants for a single macroscopic dielectric time constant, as has been briefly discussed in  
84 ref. [1].

85 Dielectric and conductivity relaxations can both occur in the same material over two  
86 resolvable frequency ranges and the usual nomenclature for the low and high frequency limits of a  
87 single relaxation process (e.g.  $\epsilon_0$  and  $\epsilon_\infty$  for the relative permittivity) is ambiguous and has  
88 caused confusion in a long standing debate about the legitimacy of the electric modulus  
89 formalism. We introduce a new nomenclature here to distinguish the low and high frequency  
90 limits for the two possible relaxations that, although somewhat clumsy, eliminates this confusion.  
91 The two limits for a dielectric relaxation at constant  $\vec{\mathbf{E}}$  are denoted by  $\epsilon_0^E$  and  $\epsilon_\infty^E$  and the two  
92 limits for a conductivity relaxation at constant  $\vec{\mathbf{D}}$  are denoted by  $\epsilon_0^D$  and  $\epsilon_\infty^D$ . Since a  
93 conductivity relaxation must in general occur at lower frequencies than a dielectric relaxation for  
94 the latter to be readily observed (with some exceptions depending on instrumental sensitivity)  
95 then  $\epsilon_\infty^D = \epsilon_0^E$ , although overlap can occur.

96 Electric charge is denoted by q (Coulomb C), volume charge density by  $\rho$  ( $\text{C m}^{-3}$ ),  
97 surface charge density by  $\sigma$   $\text{C m}^{-2}$ , linear charge density by  $\lambda$   $\text{C m}^{-1}$ , current by I (Ampere = A =  
98  $\text{C s}^{-1}$ ), current density by J ( $\text{A m}^{-2}$ ), electric potential by  $\phi_E$  ( $\text{V}=\text{JC}^{-1}$ ), electric field by E  
99 ( $\text{NC}^{-1} = \text{V m}^{-1}$ ), electric dipole moment by  $\mu_E$  (C.m), resistance by R (Ohm =  $\Omega = \text{VA}^{-1}$ ), and  
100 capacitance by C (Farad F =  $\text{CV}^{-1}$ ). The SI unit for conductance (=1/resistance) is the Siemen S  
101 (equal to  $\Omega^{-1}$ ).  
102

## 103 2.2 Electromagnetism

## 104 2.2.1 Units

105 Two systems of electromagnetic units are in use, the cgs (centimeter-gram-second) and the  
 106 MKS (meter-kilogram-second) or SI (Système Internationale). The SI system is the official  
 107 scientific system but the cgs system appears in older publications and since it is still used by  
 108 chemists and materials scientists its relationship to the SI system is delineated here. For  
 109 mechanics only the numerical value of physical quantities changes with the system of units, but in  
 110 electromagnetism there is an additional difference of approach: electric charge in the cgs system  
 111 is defined in the fundamental units mass-length-time whereas in the SI it is defined to be just as  
 112 fundamental as mass, length and time: this SI unit of charge is the Coulomb.

113 The cgs form of Coulomb's law for the force  $F$  between two point charges  $q_1$  and  $q_2$   
 114 separated by a distance  $r$  and immersed in a medium of (dimensionless) permittivity  $\varepsilon$  is  
 115

$$116 \quad F = \frac{q_1 q_2}{\varepsilon r^2}, \quad (2.1)$$

117  
 118 that gives dimensions of  $M^{1/2} L^{3/2} T^{-1}$  for the electrostatic unit (esu) of charge. The cgs equation  
 119 for the magnetic force between two straight parallel conductors of length  $L$  carrying currents  $I_1$   
 120 and  $I_2$  and separated by a distance  $r$  in a material of (dimensionless) magnetic permeability  $\mu$  is  
 121

$$122 \quad F = \frac{2\mu L I_1 I_2}{r}, \quad (2.2)$$

123  
 124 that gives dimensions of  $M^{1/2} L^{1/2}$  for the electromagnetic unit (emu) of charge. The esu and emu  
 125 units differ by a factor  $LT^{-1}$  that has the dimensions of speed and the value of the speed of light,  
 126  $c$ . This is the reason that  $c$  enters into many cgs formulae. Numerically,  $\text{emu} = c \text{esu}$  ( $c$  in cgs  
 127 units =  $2.9979 \times 10^{10}$  cm/s).

128 The Coulomb C is defined experimentally by its time derivative, the current in amperes A,  
 129 that in turn is determined using eq. (2.2). A constant  $\mu_0$  is inserted into the SI form for this  
 130 magnetic force to ensure consistency with the cgs system: the same force is produced by the same  
 131 currents separated by the same distance  
 132

$$133 \quad F = \frac{\mu\mu_0 L I_1 I_2}{4\pi r}. \quad (2.3)$$

134  
 135 Equations (2.2) and (2.3) reveal that  $\mu_0 = 4\pi \times 10^{-7} \text{ N}\cdot\text{A}^{-2}$ . The factor  $4\pi$  arises from Gauss's  
 136 Law [eq. (1.150) and eq. (2.19) below] and is a frequent source of confusion. The SI form of  
 137 Coulomb's law is  
 138

$$139 \quad F = \frac{q_1 q_2}{4\pi \varepsilon_0 \varepsilon r^2}, \quad (2.4)$$

140

141 where  $\epsilon_0$  is a constant (the permittivity of free space), with dimensions  $Q^2M^{-1}L^{-3}T^2$  that  
 142 correspond to the units of capacitance per unit length (Farads meter<sup>-1</sup>). Comparing eqs. (2.1) and  
 143 (2.4) reveals that

$$144 \quad (\text{esu})^2 = 4\pi\epsilon_0 (\text{Coulomb})^2. \quad (2.5)$$

146 The algebraic conversion between cgs and SI units for charge also needs to account for the ratio  
 147 of the different units for force ( $10^5$ ). The eventual numerical relations between C, esu and emu are  
 148  $C \approx 3 \times 10^9 \text{ esu} \approx 10^{-1} \text{ emu}$ , where the approximate equality arises from placing the speed of light  
 149 at  $3 \times 10^8 \text{ m}^{-1}$  rather than  $2.9979... \times 10^8 \text{ m}^{-1}$ . The dimensionless fine structure constant  $\alpha$  in cgs  
 150 units is  $\alpha = e^2 / \hbar c = 2\pi e^2 / hc$  (e in esu) and in SI units is  $\alpha = 2\pi e^2 / 4\pi \epsilon_0 \hbar c = e^2 / 2\epsilon_0 \hbar c$  (e in  
 151 Coulomb). It is easily confirmed that the SI value of  $\alpha$  is dimensionless and has the same  
 152 numerical value as the cgs value.

154 Having illustrated the cgs system to this point it is now dispensed with apart from one  
 155 occasional exception: the unit for the molecular dipole moment. In the SI system this is the  
 156 coulomb-meter but this unit is inconveniently large and is rarely (ever?) used. The more common  
 157 unit is the Debye, defined as the dipole moment created by two opposite charges of  $10^{-10} \text{ esu}$   
 158 ( $3.3 \times 10^{-20} \text{ C}$ ) separated by 1.0 Angstrom ( $10^{-10} \text{ m}$ ). The persistence of this unit probably  
 159 originates in the fact that molecular dipole moments are of order unity when expressed in Debyes  
 160 (D) but of order  $10^{-30}$  in coulomb-meters. It is not clear to this author why a convenient SI unit  
 161 such as  $10^{-31} \text{ C.m} \approx 0.33 \text{ D}$  or  $10^{-30} \text{ C.m} \approx 3.3 \text{ D}$  has not been introduced, especially since the  
 162 SI unit nm has replaced the Angstrom in optical spectroscopy. Perhaps indecision by the  
 163 international committee about who to name the unit after? What about Onsager (O) for example?

## 164 2.2.2 Electromagnetic Quantities

165 Many of these are conveniently defined using a parallel plate capacitor comprising two  
 166 conducting flat plates, each of area A and separated by a distance d. The geometric "cell constant"  
 167  $k$  is

$$168 \quad k \equiv d / A. \quad (2.6)$$

171 Each plate has a charge of magnitude  $q_0$  but of opposite sign (uniformly distributed since the  
 172 plates are conducting) that produces an electric potential difference  $V$  between the plates. The  
 173 capacitance is  $C \equiv q_0 / V$  that has the units unit Farad = C V<sup>-1</sup>. The surface charge density  
 174  $\sigma_0 = \pm q_0 / A$  on the plates induces an interfacial charge density  $\mp \sigma_i$  on each surface of any  
 175 dielectric material between the plates. The electric field  $\vec{E}$ , polarization  $\vec{P}$  and displacement  
 176 vector  $\vec{D}$  are perpendicular to the plates with magnitudes defined by the following table:  
 177  
 178

$$\begin{array}{ccc} 179 & \begin{array}{c} SI \\ \hline D = \sigma_0 \\ P = \sigma_i \end{array} & \begin{array}{c} cgs \\ \hline D = 4\pi \sigma_0 \\ P = \sigma_i \end{array} \\ 180 & & (2.7) \end{array}$$

$$181 \quad \begin{array}{ccc} & SI & cgs \\ & \hline & D = \sigma_0 & D = 4\pi \sigma_0 \\ & P = \sigma_i & P = \sigma_i \end{array} \quad (2.8)$$

$$182 \quad e_0 E = \sigma_0 - \sigma_i = D - P \quad E = 4\pi(\sigma_0 - \sigma_i) = D - 4\pi P \quad (2.9)$$

183  
184 The charge densities  $\sigma_0$  and  $\sigma_i$  generate an electrostatic potential  $\varphi_E$  (in volts) and net volume  
185 charge density  $\rho$  for which

$$187 \quad \vec{\mathbf{D}} = \nabla \rho \quad (2.10)$$

188  
189 and

$$191 \quad \vec{\mathbf{E}} = \nabla \varphi_E. \quad (2.11)$$

192  
193 The inverse of eq. (2.11) is

$$195 \quad \varphi_{1,2} = \int_{s_1}^{s_2} \vec{\mathbf{E}} \cdot d\vec{\mathbf{s}} \quad (2.12)$$

196  
197 where  $\varphi_{1,2}$  is the potential difference between the points  $s_1$  and  $s_2$ . The relative permittivity  $\varepsilon$   
198 and dielectric susceptibility  $\chi_d$  are defined in the following table:

$$200 \quad \begin{array}{ccc} & SI & cgs \\ & \hline 201 \quad \varepsilon \equiv \frac{D}{e_0 E} & & \varepsilon \equiv \frac{D}{E} \end{array} \quad (2.13)$$

$$202 \quad \chi_d = \frac{P}{e_0 E} = \frac{D - e_0 E}{e_0 E} = \varepsilon - 1 \quad \chi_d = \frac{P}{E} = \frac{D - E}{4\pi E} = \frac{1}{4\pi}(\varepsilon - 1) \quad (2.14)$$

203 A dielectric material between the plates decreases the electric field between the plates  
204 because the induced polarization charge density  $\sigma_i$  on the surface of the material partly cancels  
205 the unchanged charge density on the plates [eq. (2.9)]. The units of  $\mathbf{D}$  and  $\mathbf{P}$  (charge area<sup>-1</sup>)  
206 correspond to dipole moment (charge-distance) per unit volume. In view of  $\vec{\mathbf{D}}$ ,  $\vec{\mathbf{E}}$  and  $\vec{\mathbf{P}}$  being  
207 vectors the relative permittivity and dielectric susceptibility are in general tensors but for isotropic  
208 media (liquids, glasses, and isotropic crystals)  $\mathbf{D}$ ,  $\mathbf{E}$ ,  $\mathbf{P}$  and  $\varepsilon$  are all scalars. We mostly treat them  
209 as scalars in this book.

210 The magnetic analogs of  $\mathbf{D}$ ,  $\mathbf{E}$ ,  $\mathbf{P}$ ,  $e_0$ ,  $\varepsilon$  and  $\chi_d$  are, respectively, the magnetic induction  
211  $\mathbf{B}$ , the magnetic field  $\mathbf{H}$ , the magnetization  $\mathbf{M}$ , the permeability of free space,  $\mu_0$ , the relative  
212 permeability  $\mu$ , and the magnetic susceptibility  $\chi_m$ . The SI and cgs definitions are

213

$$\begin{array}{ccc}
 \text{SI} & & \text{cgs} \\
 \hline
 B = \mu_0 H & & B = H
 \end{array} \tag{2.15}$$

$$M = \frac{B}{\mu_0} - H \qquad M = \frac{B - H}{4\pi} \tag{2.16}$$

$$\mu = \frac{B}{H} \qquad \mu = \frac{B}{H} \tag{2.17}$$

$$\chi_M = \frac{M}{H} = \frac{B}{\mu_0 H} - 1 \qquad \chi_M = \frac{M}{H} = \frac{B}{4\pi H} - 1 \tag{2.18}$$

220  
 221 2.2.3 Electrostatics  
 222 Gauss's Law is  
 223

$$\oint_S \mathbf{e}_0 \varepsilon \vec{\mathbf{E}} \cdot d\vec{\mathbf{A}} = q_{\text{enclosed}} \Rightarrow \oint_S \vec{\mathbf{D}} \cdot d\vec{\mathbf{A}} = q_{\text{free}}, \tag{2.19}$$

225  
 226 where  $q_{\text{enclosed}}$  is the total net charge within a closed surface S of magnitude A,  $\varepsilon$  is the relative  
 227 permittivity of the material enclosed by the surface, and the surface integral is the flux of the  
 228 electric field through the surface. For the definition in terms of  $\vec{\mathbf{D}}$  the quantity  $q_{\text{free}}$  does not  
 229 include the induced polarization charges because these are subsumed into the permittivity  $\varepsilon_0 \varepsilon$ .  
 230 Equation (2.19) is the electrical version of the mathematical Gauss's Theorem in Chapter One [eq.  
 231 1.146]. As noted in Chapter One the differential area vector  $d\vec{\mathbf{A}}$  of a surface is defined as having  
 232 a direction perpendicular to the plane of the surface, and for closed surfaces such as occur in  
 233 Gauss's Law the outward pointing direction is defined to be positive. The Gaussian surface is a  
 234 purely mathematical object that can be placed anywhere although it must have the same symmetry  
 235 as the system under study to be helpful. Thus information about charge distribution can be  
 236 inferred even though E is determined by the total enclosed charge.

237 Gauss's Law is now used to calculate  $\vec{\mathbf{E}}$  and the capacitance C for several geometries and  
 238 charge distributions. The geometrical objects and charges are taken to be immersed in a medium  
 239 of relative permittivity  $\varepsilon$ .

240  
 241 2.2.3.1 Point Charge (Coulomb's Law)

242 Define the Gaussian surface S as a sphere of radius r with a point charge q at its center. By  
 243 symmetry  $\vec{\mathbf{E}}$  is everywhere parallel to  $d\vec{\mathbf{a}}$  and has a constant magnitude E obtained from  
 244  $q = \varepsilon_0 \varepsilon \oint \vec{\mathbf{E}} \cdot d\vec{\mathbf{A}} = 4\pi r^2 \varepsilon_0 \varepsilon E$  so that

$$E = \frac{q}{4\pi \varepsilon \varepsilon_0 r^2}. \tag{2.20}$$

247

248 2.2.3.2 Long Thin Rod with Uniform Linear Charge Density  $\lambda$ 

249 Define the Gaussian surface to be a cylinder of radius  $r$  and length  $L$ , with the rod on its  
 250 central axis. Then  $q = \epsilon\epsilon_0 \oint_S \vec{\mathbf{E}} \cdot d\vec{\mathbf{A}} = \epsilon\epsilon_0 E (2\pi r L)$  so that at a distance  $r$  from the axis

251

$$252 \quad E = \frac{\lambda}{2\pi\epsilon\epsilon_0 r}. \quad (2.21)$$

253

254 2.2.3.3 Flat Insulating Plate

255 Let a charge  $q$  be uniformly distributed over the two sides of a flat insulating plate of  
 256 "infinite area" (no edge effects) so that the charge on each surface is  $q/2$ . Define  $\sigma$  as the charge  
 257 per unit area so that the charge density on each surface is  $\sigma/2$ . Define the Gaussian surface as a  
 258 cylinder whose axis is parallel with the area vector of one side of the plate and has one end inside  
 259 the plate and the other end in a medium of relative permittivity  $\epsilon$ . Then the electric field points  
 260 away from each surface of the plate (since  $q$  is positive) and  $q/2 = \sigma A/2 = \epsilon\epsilon_0 \oint_S \vec{\mathbf{E}} \cdot d\vec{\mathbf{A}} = \epsilon\epsilon_0 EA$

261 so that

262

$$263 \quad E = \frac{\sigma}{2\epsilon_0\epsilon}. \quad (2.22)$$

264

265 This electric field is constant and independent of distance from the plate.

266

267 2.2.3.4 Flat Conducting Plate

268 Let the charge on each side of the plate be  $q/2$  and define the Gaussian surface to be the  
 269 same as that for the insulating plate in §2.2.3.3. The electrostatic field inside a conductor is zero  
 270 so that the electric field points away each surface of the plate and  
 271  $q/2 = \sigma A/2 = \epsilon_0\epsilon \oint_S \vec{\mathbf{E}} \cdot d\vec{\mathbf{A}} = \epsilon_0\epsilon EA$  so that

272

$$273 \quad E = \frac{\sigma}{2\epsilon\epsilon_0}. \quad (2.23)$$

274

275 This electric field is again constant and is also independent of distance from the plate

276

277 2.2.3.5 Two Parallel Insulating Flat Plates

278 Consider charges  $\pm q$  that are uniformly distributed over both surfaces of the plate. The  
 279 field between the plates is the vector sum of the fields from each plate. Since the field from the  
 280 positively charged plate points away from the positive plate and the field from the negatively  
 281 charged plate points toward the negative plate the two fields add up and the electric field is twice  
 282 that of eq. (2.22):

283

$$284 \quad E = \frac{\sigma}{\epsilon \epsilon_0}. \quad (2.24)$$

285

## 286 2.2.3.6 Two Parallel Conducting Flat Plates

287 Charges  $\pm q$  on each plate are attracted to the opposite charges on the other plate so that the  
 288 charges on each plate will lie totally on the inside surface and the charge density on each interior  
 289 surface is  $\sigma = q/A$ . Since the effect of one plate on the other has been taken into account in this  
 290 case the electric fields do not add up and the field between the plates is again

291

$$292 \quad E = \frac{\sigma}{\epsilon \epsilon_0}. \quad (2.25)$$

293

294 The charge density on the outer surface of each plate is zero so that the electric field outside the  
 295 plates is also zero.

296 The capacitance is obtained from the voltage difference  $V = E \cdot d$  V between the plates and  
 297  $q = A\sigma_0$ :

298

$$299 \quad C = \frac{q}{V} = \frac{\sigma_0 A}{Ed} = \frac{\sigma_0 A/d}{e_0 \epsilon / \sigma_0} = (A/d)(e_0 \epsilon) = (e_0 \epsilon / k), \quad (2.26)$$

300

301 where k is the "cell constant" corresponding to the effective A/d for the container of the dielectric.

302

## 303 2.2.3.7 Concentric Conducting Cylinders

304 Define the inner and outer radii of two concentric conducting cylindrical plates to be a and  
 305 b, respectively, let their equal height be h, and let charges +q and -q be uniformly distributed on  
 306 the inside surfaces of each plate. Consider a concentric cylindrical Gaussian surface of radius  
 307  $a < r < b$  and height h, so that  $q/e_0 \epsilon = \oint_S \vec{E} \cdot d\vec{A} = E(2\pi r h)$ . Then

308

$$309 \quad E = q / (2\pi r h e_0 \epsilon) \quad (2.27)$$

310

311 so that

312

$$313 \quad V = \int_a^b E dr = \left( \frac{q}{2\pi h e_0 \epsilon} \right) \int_a^b \frac{dr}{r} = \frac{q}{2\pi h e_0 \epsilon} \ln \left( \frac{b}{a} \right) \quad (2.28)$$

314

315 and the capacitance is

316

$$317 \quad C = \frac{q}{V} = \frac{2\pi h e_0 \epsilon}{\ln(b/a)} \quad (2.29)$$

318

## 319 2.2.3.8 Concentric Conducting Spheres

320 Define the inner and outer radii of two concentric spherical conducting plates to be  $a$  and  
 321  $b$ , respectively, and let charges  $+q$  and  $-q$  reside on the inside surfaces of each plate. Consider a  
 322 concentric spherical Gaussian surface of radius  $a < r < b$  so that  $q/e_0 = \oint_S \vec{E} \cdot d\vec{A} = E[4\pi r^2]$  and

323  $E = q/[4\epsilon_0\pi r^2]$ . Then

324

$$325 \quad V = \int_a^b E dr = \frac{q}{4\pi\epsilon_0\epsilon} \int_a^b \frac{dr}{r^2} = \frac{q}{4\pi\epsilon_0\epsilon} \left( \frac{1}{b} - \frac{1}{a} \right) = \frac{q}{4\pi\epsilon_0\epsilon} \left( \frac{a-b}{ab} \right) \quad (2.30)$$

326

327 and

$$328 \quad C = \frac{q}{V} = 4\pi\epsilon_0\epsilon \left( \frac{ab}{b-a} \right). \quad (2.31)$$

329

## 330 2.2.3.9 Isolated Sphere

331 The capacitance of an isolated sphere is obtained from eq. (2.31) by taking the limit  
 332  $b \rightarrow \infty$  and for convenience placing  $a = R$ :

333

$$334 \quad C = 4\pi\epsilon_0\epsilon R. \quad (2.32)$$

335

336 Thus larger spheres have larger capacitances.

337

## 338 2.2.4 Electrodynamics

339 Consider a constant voltage  $V$  applied across two parallel plates between which there is  
 340 now a conducting medium. Let the resistivity of the material be  $\rho = R.k^{-1}$  (units ohm-meter) and  
 341 specific conductivity  $\sigma = 1/\rho$  (units  $S\ m^{-1}$ ), where  $R$  is the resistance between the plates in ohms  
 342 and the symbol  $S$  refers to the SI unit Siemen defined as the reciprocal of the ohm. The current  
 343 density  $\vec{J}$  is the electric current per unit area (units  $A\ m^{-2}$ ) so that  $\vec{J}\rho = \vec{E}$ . Unfortunately the  
 344 displacement current  $dD/dt = d\sigma_0/dt$  (better named as the displacement current density) has no  
 345 symbol.

346 Electric current, symbol  $I$ , is defined as

347

$$348 \quad I \equiv \frac{dq}{dt} \quad (2.33)$$

349

350 so that the total charge that passes across a plane through which a current  $I$  flows is

351

$$352 \quad q = \int_0^t I dt'. \quad (2.34)$$

353

354 The electric potential  $\phi_E$  is not defined for electrodynamics (see §2.5 below on Maxwell's  
 355 equations) and is replaced by the symbol voltage  $V$  (unfortunately also used for the unit volt).  
 356 Ohm's Law for the electrical resistance  $R$  (SI unit ohm ( $\Omega$ )) is then

$$357$$

$$358 \quad R \equiv \frac{V}{I} \quad (2.35)$$

359 and  $\Omega = V / A$ . An electrical conductor is said to be ohmic if, and only if,  $R$  is constant. This is  
 360 not the same as  $dV/dI = \text{constant}$ : for example if  $V = 1.0 + 2I$  so that  $dV/dI = 2$  then  
 361  $R = 3\Omega$  for  $I = 1A$ ,  $R = 2.5\Omega$  for  $I = 2A$ ,  $R = 2.3\Omega$  for  $I = 3A$ .

362 Resistances dissipate power  $P$  given by  $P = IV$  (recall that energy is given by  $QV$  and  
 363 power is the time derivative of energy). For ohmic resistances

$$364$$

$$365 \quad P = IV$$

$$366 \quad = I(IR) = I^2R \quad (2.36)$$

$$= (V/R)V = V^2/R.$$

### 367 2.2.5 Maxwell's Equations

368 These four equations summarize all that is known about electromagnetic phenomena –  
 369 they are essentially the electromagnetic equivalent of Newton's laws for mechanics but are more  
 370 mathematically sophisticated because of the greater complexity of electromagnetic phenomena.

371 The differential forms of the four Maxwell equations are:

$$372$$

$$373 \quad \vec{\nabla} \cdot \vec{\mathbf{D}} = \rho; \quad (2.37)$$

$$374 \quad \vec{\nabla} \cdot \vec{\mathbf{B}} = 0; \quad (2.38)$$

$$375 \quad \vec{\nabla} \times \vec{\mathbf{E}} = -\left(\frac{\partial \vec{\mathbf{B}}}{\partial t}\right); \quad (2.39)$$

$$376 \quad \vec{\nabla} \times \vec{\mathbf{H}} = \vec{\mathbf{J}} + \left(\frac{\partial \vec{\mathbf{D}}}{\partial t}\right) \quad (2.40)$$

$$377 \quad = \sigma \vec{\mathbf{E}} + \left(\frac{\partial \vec{\mathbf{D}}}{\partial t}\right) \quad (2.41)$$

$$378 \quad = \sigma \vec{\mathbf{E}} + \epsilon_0 \left(\frac{\partial \epsilon \vec{\mathbf{E}}}{\partial t}\right). \quad (2.42)$$

379 Equation (2.40) for a vacuum is equivalent to

$$380$$

$$381 \quad \vec{\nabla} \times \vec{\mathbf{B}} = \mu_0 \vec{\mathbf{J}} + \mu_0 \epsilon_0 \left(\frac{\partial \vec{\mathbf{E}}}{\partial t}\right), \quad (2.43)$$

384 where  $\sigma$  is the specific electrical conductivity (units  $(\Omega^{-1}\text{m}^{-1} = \text{Sm}^{-1})$ ),  $\vec{\mathbf{B}}$  is the magnetic  
 385 induction, and  $\vec{\mathbf{H}}$  is the magnetic field. Equations (2.40) - (2.42) merit some discussion. The  
 386 equation  $\vec{\nabla} \times \vec{\mathbf{H}} = \vec{\mathbf{J}}$  might perhaps be expected instead of eq. (2.40) but this has the nonsensical  
 387 implication that there could never be any sources or sinks of current anywhere at any time,  
 388 because the vector identity  $\vec{\nabla} \cdot (\vec{\nabla} \times \vec{\mathbf{H}}) = 0$  would then imply  $\vec{\nabla} \cdot \vec{\mathbf{J}} = 0$ . The difficulty is resolved  
 389 by noting that for a charging or discharging parallel plate capacitor (for example) charge flow in  
 390 the external circuit joining the two capacitor plates, corresponding to  $dq_0/dt$  where  $q_0$  is the  
 391 charge on the capacitor plates (see §2.1.2 above), must be compensated for by an opposite change  
 392 of the polarization charges between the plates (to ensure charge conservation). Thus  
 393

$$394 \quad \vec{\nabla} \cdot (\vec{\nabla} \times \vec{\mathbf{H}}) \equiv 0 = \vec{\nabla} \cdot \left[ \left( \frac{\partial q_0}{\partial t} \right) - \left( \frac{\partial q_i}{\partial t} \right) \right] \quad (2.44)$$

395 is ensured.

396 The term  $\partial \vec{\mathbf{D}} / \partial t$  in eq. (2.40) can correspond for example to a localized (molecular  
 397 diameter) effective spatial translation of charge due to rotation of an electric dipole about its  
 398 center of mass that has a close analogy to an ion hopping to an adjacent site (see §2.2.1.2). It is  
 399 called the displacement current. The term displacement “current” has been claimed to be a  
 400 misnomer but this is true only if a current is interpreted to be a long range translational migration  
 401 of charge. If the definition of current as  $dq/dt$  is adopted it is not a misnomer because  $q$  (on  
 402 capacitor plates for example) changes with time [eq. (2.44)], and furthermore a traditional current  
 403 must be present in an external circuit to compensate for  $\partial q_i / \partial t$ . Describing  $\partial \vec{\mathbf{D}} / \partial t$  as a  
 404 “fictitious current”, as has been done in at least one popular text book, is disingenuous and  
 405 misleading because eq. (2.40) demonstrates that  $\partial \vec{\mathbf{D}} / \partial t$  is just as important in determining a  
 406 magnetic field as migration of individual charges.

407 The vector potential  $\vec{\mathbf{A}}$  is defined by

$$408 \quad \vec{\nabla} \times \vec{\mathbf{A}} = \vec{\mathbf{B}} \quad (2.45)$$

410 and  
 411

$$412 \quad \vec{\mathbf{E}} = -\vec{\nabla} \varphi_E - \frac{\partial \vec{\mathbf{A}}}{\partial t}, \quad (2.46)$$

414 and essentially ensures consistency between electrostatics and electrodynamics. Equation (2.45)  
 415 ensures eq. (2.38) because of the vector identity  $\vec{\nabla} \cdot (\vec{\nabla} \times \vec{\mathbf{A}}) = 0$  and eqs. (2.45) and (2.46)  
 416 together ensure that eq. (2.39) remains true in dynamic situations where  $\varphi_E$  is undefined. The  
 417 vector potential is essentially an extension of the Coulomb potential  $\varphi_E$  to dynamic situations  
 418 because the definition of  $\varphi_E$  from  $\vec{\mathbf{E}} = \nabla \varphi_E$  [eq. (2.11)] is definable only in static situations, as the  
 419

420 following consideration indicates: if  $\partial \vec{\mathbf{B}} / \partial t \neq 0$  then  $\vec{\nabla} \times \vec{\mathbf{E}} \neq 0$  by eq. (2.38) and the static  
421 relation

422

$$423 \quad \vec{\mathbf{E}} = \vec{\nabla} \varphi_E \quad (2.47)$$

424

425 could then never hold because of the vector identity  $\vec{\nabla} \times (\vec{\nabla} \varphi_E) = 0$ . But  $\vec{\mathbf{E}}$  is known to be

426 nonzero in dynamic situations (hence currents). Similarly if  $\vec{\mathbf{J}} \neq 0$  or  $\partial \vec{\mathbf{D}} / \partial t \neq 0$  then there is

427 no potential  $\varphi_B$  for  $\vec{\mathbf{B}}$  (defined by  $\vec{\mathbf{B}} = \vec{\nabla} \varphi_B$ ) because eq. (2.40) then implies

428  $\vec{\nabla} \times \vec{\mathbf{H}} = \vec{\nabla} \times \vec{\mathbf{B}} / \mu \mu_0 \neq 0$  because of the same vector identity  $\vec{\nabla} \times (\vec{\nabla} \varphi_B) = 0$ . Both of these

429 difficulties are averted by the introduction of  $\vec{\mathbf{A}}$ . Equation (2.46) is then consistent with eq.

430 (2.39) since it guarantees

431

$$432 \quad \vec{\nabla} \times \vec{\mathbf{E}} = \vec{\nabla} \times \left( -\vec{\nabla} \varphi_E - \frac{\partial \vec{\mathbf{A}}}{\partial t} \right) = -\frac{\partial \vec{\mathbf{B}}}{\partial t}. \quad (2.48)$$

433

434 Integral versions of Maxwell's equations include Faraday's Law:

435

$$436 \quad \oint \vec{\mathbf{E}} \cdot d\vec{\mathbf{s}} = -\frac{d\Phi_B}{dt}; \quad \Phi_B \equiv \oint \vec{\mathbf{B}} \cdot d\vec{\mathbf{A}} = \text{magnetic flux} \quad (2.49)$$

437

438 and Ampere's law

439

$$440 \quad \oint \vec{\mathbf{B}} \cdot d\vec{\mathbf{s}} = \mu_0 \epsilon_0 \frac{d\Phi_E}{dt} + \mu_0 I_{\text{enclosed}}; \quad \Phi_E \equiv \oint \vec{\mathbf{E}} \cdot d\vec{\mathbf{A}} = \text{electric flux}. \quad (2.50)$$

441

442 Equation (2.42) provides a convenient demonstration of the equivalence of the complex

443 permittivity and complex conductivity. First convert eq. (2.42) from a vector equation to a

444 complex scalar equation:

445

$$446 \quad \vec{\nabla} \times \vec{\mathbf{H}} = \sigma \vec{\mathbf{E}} + \epsilon_0 \left( \frac{\partial \epsilon \vec{\mathbf{E}}}{\partial t} \right) \Rightarrow |\vec{\nabla} \times \vec{\mathbf{H}}| = \sigma^* E^* + \epsilon_0 \epsilon^* \left( \frac{\partial E^*}{\partial t} \right). \quad (2.51)$$

447

448 For a sinusoidal excitation  $E^* = E_0 \exp(-i\omega t)$  eq. (2.51) becomes

449

$$\begin{aligned} |\vec{\nabla} \times \vec{\mathbf{H}}| &= \sigma^* E_0 \exp(-i\omega t) - \epsilon_0 \epsilon^* E_0 (i\omega) \exp(-i\omega t) \\ 450 \quad &= [\sigma^* - i\omega \epsilon_0 \epsilon^*] E_0 \exp(-i\omega t) \\ &= [\epsilon^* - \sigma^* / (i\omega \epsilon_0)] (-i\epsilon_0 \omega) E_0 \exp(-i\omega t), \end{aligned} \quad (2.52)$$

451

452 indicating that both the complex conductivity  $[\sigma^* - i\omega\epsilon_0\epsilon^*]$  and complex permittivity  
 453  $[\epsilon^* - \sigma^*/(i\omega\epsilon_0)]$  provide equivalent descriptions of electrical relaxation, as do the resistivity  
 454  $\rho^* = 1/\sigma^*$  and electric modulus  $M^* = 1/\epsilon^*$ . All these different functions emphasize or suppress  
 455 different facets of experimental data in the same way that Fourier transforms do for example [see  
 456 eq. (2.106) below].

## 457 2.2.6 Electromagnetic Waves

459 The Maxwell equations together with the constitutive relations  $\vec{D} = \epsilon_0\epsilon\vec{E}$  and  $\vec{B} = \mu_0\mu\vec{H}$   
 460 predict transverse electromagnetic (em) waves traveling at the speed of light  $c/n$  given by  
 461

$$462 \frac{c}{n} = \frac{(1/\epsilon_0\mu_0)^{1/2}}{(\epsilon\mu)^{1/2}} = \frac{1}{(\epsilon_0\epsilon\mu_0\mu)^{1/2}}, \quad (2.53)$$

463 where  
 464

$$466 n = (\epsilon\mu)^{1/2} \quad (2.54)$$

467 is the refractive index. In a nonmagnetic material for which  $\mu = 1$  and  $\epsilon^* = (n^*)^2$   
 468

$$470 (n^*)^2 = (n' - in'')^2 = (n'^2 - n''^2) - 2in'n'' = \epsilon^* = \epsilon' - i\epsilon'' \quad (2.55)$$

471 so that  
 472

$$474 \epsilon' = n'^2 - n''^2 \quad (2.56)$$

475 and  
 476

$$478 \epsilon'' = 2n'n''. \quad (2.57)$$

480 For the general case of a magnetic material where the relative magnetic permeability is also  
 481 complex,  $\mu^* = \mu' - i\mu''$ ,

$$483 (n^*)^2 = (n'^2 - n''^2) - 2in'n'' = (\epsilon' - i\epsilon'')(\mu' - i\mu'') \quad (2.58)$$

484 so that  
 485

$$487 (n^*)^2 = (n'^2 - n''^2) - 2in'n'' = (\epsilon' - i\epsilon'')(\mu' - i\mu'') = (\epsilon'\mu' - \epsilon''\mu'') - i(\epsilon'\mu'' + \epsilon''\mu'), \quad (2.59)$$

488 and  
 489

490

$$491 \quad n'' = (\varepsilon' \mu'' + \varepsilon'' \mu'). \quad (2.60)$$

492

493 Thus absorption of electromagnetic energy by magnetically lossy materials is enhanced by a high  
494 relative permittivity and dielectric loss is enhanced in magnetic materials.

495 The electric field component of a plane electromagnetic traveling wave of angular  
496 frequency  $\omega$  propagating in the +x direction in a medium with refractive index  $n$  and speed  $c/n$  is

$$497 \quad E(x, t) = E_0 \exp \left\{ -i\omega \left[ t - \frac{nx}{c} \right] \right\}, \quad (2.61)$$

498

499 and similarly for the magnetic field component. For complex  $n^* = n' - in''$  eq. (2.61) becomes

500

$$501 \quad \begin{aligned} E(x, t) &= E_0 \exp \left\{ -i\omega \left[ t - \frac{(n' - in'')x}{c} \right] \right\} \\ &= E_0 \exp \left\{ -i\omega \left[ t - \frac{n'x}{c} \right] \right\} \exp \left[ \frac{-n''\omega x}{c} \right], \end{aligned} \quad (2.62)$$

502

503 so that  $E$  decays exponentially with distance +x into the medium. The intensity  $I = |E|^2$  of em  
504 waves is then

505

$$506 \quad \begin{aligned} I &= E_0^2 \exp \left\{ -2i\omega \left[ t - \frac{(n' - in'')x}{c} \right] \right\} \\ &= E_0^2 \exp \left\{ -2i\omega \left[ t - \frac{n'x}{c} \right] \right\} \exp \left[ \frac{-2n''\omega x}{c} \right], \end{aligned} \quad (2.63)$$

507

508 that is to be compared with Beer's Law

509

$$510 \quad I = I_0 \exp(-\alpha x), \quad (2.64)$$

511

512 where  $\alpha$  is the extinction coefficient (usually expressed in neper  $m^{-1}$  where the dimensionless  
513 neper is used to emphasize the fact that the logarithmic form of eq. (2.64) implies the Naperian  
514 logarithm). Equations (2.63) and (2.64) yield

515

$$516 \quad \alpha(\omega) = \frac{2\omega n''(\omega)}{c}. \quad (2.65)$$

517

518 The sign convention for imaginary numbers mentioned in the Introduction of Chapter One  
519 is seen to be at work here. If the sinusoidal perturbation was defined as

520  $E(x,t) = E_0 \exp\{+i\omega[t - nx/c]\}$  and the sign of the imaginary component of  $\varepsilon^*$  remained  
 521 negative then  $\alpha$  would have to be negative and Beer's Law would predict unphysical exponential  
 522 growth through a medium. This can be resolved by making the imaginary component of  $\varepsilon^*$   
 523 positive but this corresponds to a dipole rotation that leads the excitation voltage rather than lags  
 524 it. Nonetheless this is the convention used by electrical engineers and is the price paid for the  
 525 "advantage" of having a positive sign in the complex exponential. An excellent account of phase  
 526 conventions is given in Chapter One of ref. [2].

527 Insertion of eq. (2.57) into eq. (2.65) yields

$$529 \quad \alpha(\omega) = \frac{\omega\varepsilon''(\omega)}{n'(\omega)c}, \quad (2.66)$$

530  
 531 and since  $\varepsilon'' = \sigma'/(e_0\omega)$  then

$$533 \quad \alpha(\omega) = \frac{\sigma'(\omega)}{n'(\omega)e_0c}. \quad (2.67)$$

534  
 535 Thus  $n''$ ,  $\varepsilon''$ ,  $\alpha$  and  $\sigma'$  are all measures of absorption of electrical energy:

$$537 \quad \alpha = \frac{\sigma'}{ne_0c} = \frac{\omega\varepsilon''}{nc} = \frac{2\omega n''}{c}. \quad (2.68)$$

538  
 539 Ordinary em radiation comprises randomly distributed directions of polarization for the  $\vec{\mathbf{E}}$   
 540 and  $\vec{\mathbf{B}}$  fields (that are always perpendicular to one another). Radiation for which the direction of  
 541 polarization is constant and the same for all waves is said to be polarized. Reflected em waves are  
 542 partially polarized in the direction parallel to the reflecting surface, the extent of polarization  
 543 depending on the angle of incidence. Polaroid® sun glasses are polarized in the vertical direction  
 544 and therefore more strongly attenuate reflected waves. Reflected em waves are fully polarized at  
 545 the Brewster incident angle.

#### 547 2.2.7 Local Electric Fields

548 The electric field inside a dielectric medium is not equal to the applied field because of  
 549 electrostatic screening by the medium. This is a complicated problem that is well described in  
 550 Chapter One of ref. [3] (by N. E. Hill) and has been considered by Onsager [4], Kirkwood [5],  
 551 and Frohlich [6]. The complexity of the issue is illustrated by the Kirkwood relation between the  
 552 isolated molecular dipole moment  $\mu_g$  observed in the gas phase and the relative permittivity  $\varepsilon_0^E$

$$554 \quad \frac{4\pi Ng\mu_g^2}{9k_B T V \varepsilon_0} = \frac{(\varepsilon_0^E - \varepsilon_\infty^E)(2\varepsilon_0^E + \varepsilon_\infty^E)}{\varepsilon_0^E(\varepsilon_\infty^E + 2)}, \quad (2.69)$$

555

556 where  $\epsilon_\infty^E$  is the limiting high frequency relative permittivity that for a pure dielectric equals the  
 557 square of the (limiting low frequency) refractive index  $n^2$ ,  $N$  is the number of dipoles in a volume  
 558  $V$ , and  $g$  is a correlation factor that corrects for nonrandom orientations of surrounding dipoles  
 559 caused by direction dependent intermolecular forces. The latter is in principle calculable:  
 560

$$561 \quad g = 1 + \sum_{i \neq j}^N \langle \cos(\theta_{ij}) \rangle, \quad (2.70)$$

562  
 563 where the averaged cosine  $\langle \cos(\theta_{ij}) \rangle$  of the angle  $\theta_{ij}$  between dipoles  $\mu_i$  and  $\mu_j$  can be  
 564 computed for specific orientation geometries.

565 The treatment of local field effects on the kinetics of dipole relaxation is even more  
 566 intricate because the reaction field produced by polarization of the dielectric medium by the  
 567 embedded dipole is in general out of phase with the applied field. These effects have been  
 568 discussed by Mountain [7]. A particularly important effect of local fields on relaxation  
 569 phenomenology is that a single macroscopic dielectric relaxation time corresponds to two  
 570 microscopic times. After a heated debate in the literature the accepted microscopic dipole  
 571 correlation function is the Fatuzzo and Mason [8] expression  
 572

$$573 \quad \begin{aligned} \varphi(t) &= \left(1 + \frac{\epsilon_\infty}{2\epsilon_0}\right)^{-1} \left[ \exp\left(-\frac{t}{\tau_E}\right) + \left(\frac{\epsilon_\infty}{2\epsilon_0}\right) \exp\left(-\frac{\epsilon_0}{\epsilon_\infty} \frac{t}{\tau_E}\right) \right] \\ &= \left(1 + \frac{\epsilon_\infty}{2\epsilon_0}\right)^{-1} \left[ \exp\left(-\frac{t}{\tau_E}\right) + \left(\frac{\epsilon_\infty}{2\epsilon_0}\right) \exp\left(-\frac{t}{\tau_D}\right) \right], \end{aligned} \quad (2.71)$$

574  
 575 where  $\tau_E$  and  $\tau_D$  are again the relaxation times for polarization at constant E and D respectively.  
 576 Fulton [9] has given a detailed discussion of this subject in which he deduced that the longitudinal  
 577 part of polarization relaxes with a time constant  $\tau_D$  and that the transverse component relaxes  
 578 with a time constant  $\tau_E$ . Electrical relaxation is therefore discussed later in this chapter in two  
 579 parts - dielectric relaxation and conductivity relaxation.  
 580

## 581 2.2.8 Circuits

582 There are the four fundamental elements in analog passive circuits: resistance R;  
 583 capacitance C; self inductance L; mutual inductance M.  
 584

### 585 2.2.8.1 Simple Circuits

#### 586 Resistances in Series and in Parallel

587 For resistances  $R_i$  connected in series the same current  $I$  must pass through each and the  
 588 sum of the voltages across each resistor equals the applied voltage. Thus  $V = \sum V_i = I \sum R_i = IR_s$   
 589 and the equivalent series resistance  $R_s$  is  
 590

$$591 \quad R_s = \sum R_i . \quad (2.72)$$

592  
 593 For resistances  $R_i$  connected in parallel the same voltage  $V$  must occur across each and  
 594 the total current  $I$  through the parallel circuit is the sum of the currents through each  
 595 resistance:  $I = \sum I_i = \sum V / R_i$  so that the equivalent parallel resistance  $R_p$  is given by

$$596 \quad 1/R_p = \sum 1/R_i . \quad (2.73)$$

597  
 598  
 599 Capacitances in Series and in Parallel

600 Capacitance  $C$  is defined as  $C = q/V$ , where  $V$  is the voltage across the capacitor and  $\pm q$   
 601 are the charges on each of its ends. For capacitances  $C_i$  connected in parallel the same voltage  
 602  $V$  must occur across each and the total charge  $q$  on each side of the equivalent parallel  
 603 capacitance  $C_p$  must equal the sum of charges  $q_i$  on each component. Thus

604  $q = \sum_i q_i = V \sum_i C_i = C_p V$  and the equivalent parallel capacitance  $C_p$  is given by

$$605 \quad C_p = \sum_i C_i . \quad (2.74)$$

606  
 607 For capacitances connected in series the total voltage  $V$  across the series circuit equals the  
 608 sum of voltages across each capacitor. The magnitude of the charges  $q$  on each must be the same  
 609 (since no charge separation can occur across the short circuit joining them) so that  
 610  $V = q / C_s = \sum_i V_i = \sum_i q / C_i$  and the equivalent series capacitance  $C_s$  is given by

$$611 \quad \frac{1}{C_s} = \sum_i \frac{1}{C_i} . \quad (2.75)$$

612  
 613  
 614 Inductances in Series and in Parallel

615 The self-inductance  $L$  is defined as  $L \equiv V / (dI / dt)$  where  $V$  is the voltage across the  
 616 device and  $I$  is the current through it. Since  $V$  is in the numerator and  $I$  is in the denominator  $L$  is  
 617 an impedance akin to  $R$ . Impedances add in series so the equivalent series inductance  $L_s$  is

$$618 \quad L_s = \sum_i L_i , \quad (2.76)$$

619  
 620 and since admittances add in parallel the equivalent parallel inductance  $I_p$  is

$$621 \quad \frac{1}{L_s} = \sum_i \frac{1}{L_i} \quad (2.77)$$

622  
 623  
 624  
 625

626 For the sake of completion the mutual inductance  $M$  is now described although for reasons  
 627 given below it rarely comes into play for relaxation phenomena or instrumentation. It is defined as  
 628  $M = V_2 / (dI_1 / dt)$ , where  $V_2$  is the voltage induced on one side of the device by a time varying  
 629 current  $I_1$  in the other. Rearrangement of this definition of  $M$  yields

$$631 \quad V_2 = M (dI_1 / dt), \quad (2.78)$$

632  
 633 so that  $V_2$  is smaller at lower frequencies when  $dI_1/dt$  is smaller. This is why transformer arm (ac  
 634 Wheatstone) bridges are useless at low frequencies. Series and parallel combinations of mutual  
 635 inductances add up in the same way as self inductances.

### 636 Combined Series and Parallel Elements

637 Consider two examples of a circuit in which an element  $Z_1$  is in parallel with a series  
 638 combination of two elements  $Z_2$  and  $Z_3$ . If these elements are resistances  $R_1$ ,  $R_2$  and  $R_3$  then  
 639  $R_{23} = R_2 + R_3$  and

$$641 \quad \frac{1}{R_{equiv}} = \frac{1}{R_1} + \frac{1}{R_2 + R_3} = \frac{R_1 + R_2 + R_3}{R_1(R_2 + R_3)} \quad (2.79)$$

642  
 643 or

$$644 \quad R_{equiv} = \frac{R_1(R_2 + R_3)}{R_1 + R_2 + R_3}. \quad (2.80)$$

645  
 646 If these elements are capacitances  $C_1$ ,  $C_2$  and  $C_3$  then  
 647  $1/C_{23} = 1/C_2 + 1/C_3 \Rightarrow C_{23} = C_2 C_3 / (C_2 + C_3)$  and

$$648 \quad C_{equiv} = C_1 + C_{23} = C_1 + \frac{C_2 C_3}{C_2 + C_3} = \frac{C_1 C_2 + C_2 C_3 + C_3 C_1}{C_2 + C_3}. \quad (2.81)$$

### 652 2.2.8.2 AC Circuits

653 If a voltage  $V(t) = V_0 \cos(\omega t) = \text{Re}[V_0 \exp(-i\omega t)]$  is applied across a circuit the average  
 654 voltage over one period is zero but the ac power is not. Equation (2.36) indicates that power is  
 655 determined by the averages of  $I^2$  and  $V^2$  that are both proportional to the averages of  $\sin^2(\omega t)$  or  
 656  $\cos^2(\omega t)$  over one cycle that are both equal to  $1/2$ . Thus

$$657 \quad P_{average} = (V_0^2 / 2) R = I_0^2 R / 2. \quad (2.82)$$

658  
 659 The ac power dissipation is therefore given by the same relation for DC power dissipation if the  
 660  
 661

662 maximum ac voltage ( $V_0$ ) and current ( $I_0$ ) are replaced by  $V_0/2^{1/2}$  and  $I_0/2^{1/2}$  respectively. The  
 663 latter are referred to as rms (root mean square) voltages and currents. Electrical outlet ac voltages  
 664 such as 120V in North America are given as rms values; the peak voltage in North America is  
 665 therefore  $(120V)(2)^{1/2} = 170V$ .

666 AC impedances  $Z^*(i\omega)$  are defined as  $V^*(i\omega)/I^*(i\omega)$  and ac admittances  $A^*(i\omega)$  as  
 667  $I^*(i\omega)/V^*(i\omega)$ . The imaginary components of  $A^*(i\omega)$  and  $Z^*(i\omega)$  are referred to as  
 668 reactances, and as shown below do not dissipate power.

### 669 Resistances

670 For a voltage  $V = V_0 \exp(-i\omega t)$  applied across a resistance R the current is

$$671 \quad I_R(i\omega) = \frac{V(i\omega)}{R} = \frac{V_0}{R} \exp(-i\omega t) = V_0 G \exp(-i\omega t) \quad (2.83)$$

672 so that the impedance is

$$673 \quad Z_R^*(i\omega) = \frac{V^*(i\omega)}{I^*(i\omega)} = \frac{V_0 \exp(-i\omega t)}{(V_0/R) \exp(-i\omega t)} = R \quad (2.84)$$

674 and the admittance  $A_R^*(i\omega) = 1/Z_R^*(i\omega) = G$  where G is the conductance. Both R and G are real  
 675 and independent of frequency.

### 681 Capacitances

682 For a capacitance C the current is

$$683 \quad I_C(i\omega) = \frac{dq(\omega t)}{dt} = C \frac{dV(i\omega t)}{dt} = V_0 [-i\omega C \exp(-i\omega t)], \quad (2.85)$$

684 the capacitive impedance is

$$685 \quad Z_C^*(i\omega) = \frac{V^*(i\omega)}{I_C^*(i\omega)} = \frac{V_0 \exp(-i\omega t)}{V_0 [-i\omega \exp(-i\omega t)]} = \frac{1}{-i\omega C} = \frac{i}{\omega C}, \quad (2.86)$$

686 the capacitive admittance is

$$687 \quad A_C^*(i\omega) = -i\omega C. \quad (2.87)$$

694  
 695 The capacitive admittance and admittance are therefore frequency dependent and imaginary.  
 696 Power dissipation per cycle in a capacitance is given by  
 697

$$\begin{aligned}
 P_C(t) &= \langle V_C(t) I_C(t) \rangle = \langle [V_0 \exp(-i\omega t)] V_0 [-i\omega C_p \exp(-i\omega t)] \rangle = -V_0^2 \omega C_p \langle \exp(-2i\omega t) \rangle \\
 &= \langle -V_0^2 \omega C_p [\cos(-2\omega t) - i \sin(-2\omega t)] \rangle \\
 &= \langle -V_0^2 \omega C_p [\cos(2\omega t) + i \sin(2\omega t)] \rangle \\
 &= 0
 \end{aligned} \tag{2.88}$$

699 because the averages of both  $\cos(2\omega t)$  and  $\sin(2\omega t)$  over one cycle are zero. The capacitive  
 700 impedance is therefore not a resistance if "resistance" is taken to imply power dissipation. This is  
 701 why an inductive or capacitive impedance is not considered to be an "ac resistance".  
 702  
 703

#### 704 *Inductances*

705 For a self-inductance L the current is  
 706

$$I_L(\omega t) = \int \left( \frac{V}{L} \right) dt = \int \left( \frac{V_0 \exp(-i\omega t)}{L} \right) dt = \left( \frac{V_0}{L} \right) \frac{\exp(-i\omega t)}{-i\omega} \tag{2.89}$$

708 so that inductive impedance is  
 709  
 710

$$Z_L^*(i\omega t) = \frac{V^*(i\omega t)}{I_L^*(i\omega t)} = -i\omega L \tag{2.90}$$

712 and the inductive admittance is  
 713  
 714

$$A_L^*(i\omega t) = \frac{1}{-i\omega L} = \frac{i}{\omega L} . \tag{2.91}$$

716 The inductive reactance is therefore also imaginary and frequency dependent. Power dissipation  
 717 in an inductance is given by  
 718  
 719

$$\begin{aligned}
 P_L(t) &= \langle V_L(t) I_L(t) \rangle = \left\langle [V_0 \exp(-i\omega t)] \left( \frac{V_0}{L} \right) \frac{\exp(-i\omega t)}{-i\omega} \right\rangle \\
 &= -\frac{V_0^2}{i\omega L} \langle \exp(-2i\omega t) \rangle = \frac{V_0^2}{i\omega L} \langle \exp(-2i\omega t) \rangle = 0.
 \end{aligned} \tag{2.92}$$

721 Thus the power dissipated by an inductance with no resistance is zero, just like that of a  
 722 capacitance.  
 723  
 724

725 *Parallel Resistance and Capacitance*

726 Consider a voltage  $V = V_0 \cos(\omega t)$  applied across a resistance  $R_p$  in parallel with a  
 727 capacitance  $C_p$ . The current  $I_R$  through the resistance is  
 728

$$729 \quad I_R = \frac{V}{R_p} = \frac{V_0 \cos(\omega t)}{R_p} = V_0 \cos(\omega t) G_p = \operatorname{Re} [V_0 G_p \exp(-i\omega t)] \quad (2.93)$$

730 where  $G_p = 1/R_p$  is the conductance. The current through the capacitance  $I_C$  is  
 731  
 732

$$733 \quad I_C = \frac{dq_C}{dt} = C_p \frac{dV}{dt} = -V_0 \omega C_p \sin(\omega t) \quad (2.94)$$

$$= -V_0 \omega C_p \cos(\omega t - \pi/2) \operatorname{Re} [-iV_0 \omega C_p \exp(-i\omega t)]$$

734 where  $q_C$  is the charge on the capacitor. Equation (2.94) implies that the sinusoidal (displacement)  
 735 current  $I_C$  lags the applied voltage by  $\pi/2$  radians because  $\sin(\omega t) = \cos(\omega t - \pi/2)$ . The total  
 736 current through the parallel  $R_p C_p$  circuit is  
 737  
 738

$$739 \quad I = I_R + I_C = V_0 G_p \cos(\omega t) - V_0 \omega C_p \sin(\omega t)$$

$$= \operatorname{Re} [V_0 G_p \exp(-i\omega t)] + \operatorname{Re} [-iV_0 \omega C_p \exp(-i\omega t)] \quad (2.95)$$

$$= \operatorname{Re} \{V_0 [G_p - i\omega C_p] \exp(-i\omega t)\}.$$

740 The phase relations for the current are therefore conveniently expressed by defining the parallel  
 741 combination of resistance and capacitance as a complex admittance  $A^*$   
 742  
 743

$$744 \quad A^* = G_p - i\omega C_p, \quad (2.96)$$

745 or as a complex impedance  $Z^*$   
 746  
 747

$$748 \quad Z^* = 1/A^* = \frac{1}{G_p - i\omega C_p} = \frac{G_p}{G_p^2 + \omega^2 C_p^2} + \frac{i\omega C_p}{G_p^2 + \omega^2 C_p^2}. \quad (2.97)$$

749 The complex capacitance is  
 750  
 751

$$752 \quad C^* = \frac{A^*}{-i\omega} = C_p + \frac{iG_p}{\omega} \quad (2.98)$$

753 and the complex electric modulus is  
 754  
 755

$$756 \quad M^*(i\omega) = 1/C^*(i\omega) = i\omega Z^*(i\omega). \quad (2.99)$$

757  
758  
759

Equation (2.97) is equivalent to

$$Z^* = \frac{R_p}{1 + \omega^2 \tau_D^2} + \frac{iR_p \omega \tau_D}{1 + \omega^2 \tau_D^2} \quad (2.100)$$

761  
762  
763

where

$$\tau_D = R_p C_p \quad (2.101)$$

765

is the Maxwell relaxation time (the reason for the subscript  $D$  is given below).

766 When normalized by the cell constant  $k$  (dimensions  $m^{-1}$ ) the quantities  $A^*$ ,  $Z^*$  and  $C^*$  and  
767  $M^*$  become respectively the complex conductivity  $\sigma^* = kA^*$ , complex resistivity  $\rho^* = Z^*/k$ ,  
768 complex relative permittivity  $\varepsilon^* = kC^*/\epsilon_0 = C^*/C_0$  (where  $C_0$  is the capacitance of the  
769 measuring cell in a vacuum, usually equated to that in air), and complex modulus  $M^*$ . Historically  
770 the same symbol has been used for the complex electric modulus defined in terms of measured  
771 circuit elements and as a material property, but this has not caused much (any?) confusion  
772 probably because the inverse capacitance  $V/q$  has never been considered as a physically useful  
773 quantity (in this respect it is not clear to this author why conductivity and resistivity should have  
774 separate physical identities either).

775

#### 776 *Series Resistance and Capacitance*

777  
778  
779

For a resistance  $R_s$  in series with a capacitance  $C_s$

$$Z^*(i\omega) = R_s + \frac{1}{i\omega C_s} = R_s - \frac{i}{\omega C_s} = R_s \left( \frac{\omega \tau_E - i}{\omega \tau_E} \right), \quad (2.102)$$

781

$$A^*(i\omega) = \frac{R_s}{1 + \omega^2 R_s^2 C_s^2} + \frac{i\omega R_s^2 C_s}{1 + \omega^2 R_s^2 C_s^2} = \frac{R_s}{1 + \omega^2 \tau_E^2} + \frac{i\omega R_s \tau_E}{1 + \omega^2 \tau_E^2}, \quad (2.103)$$

783

$$C^*(i\omega) = \frac{A^*(i\omega)}{-i\omega} = C_s \left( \frac{1 - i\omega R_s C_s}{1 + \omega^2 R_s^2 C_s^2} \right) = C_s \left( \frac{1}{1 + \omega^2 \tau_E^2} - \frac{i\omega \tau_E}{1 + \omega^2 \tau_E^2} \right), \quad (2.104)$$

785

$$M^*(i\omega) = i\omega Z^*(i\omega) = i\omega \left( R_s - \frac{i}{\omega C_s} \right) = i\omega R_s \left( \frac{\omega \tau_E - i}{\omega \tau_E} \right) = \frac{R_s}{\tau_E} (1 + i\omega \tau_E) \quad (2.105)$$

787

788 where  $\tau_E = R_s C_s$  that is generally not equal to  $\tau_D = R_p C_p$ .

789

The relations between the four response functions are conveniently summarized by [1,10]

790

$$\begin{array}{ccc}
\varepsilon^*(i\omega) & \Leftrightarrow & 1/M^*(i\omega) \\
\Downarrow & & \Downarrow \\
\sigma^*(i\omega)/(ie_0\omega) & \Leftrightarrow & ie_0\omega/\rho^*(i\omega)
\end{array} \quad (2.106)$$

792

## 793 2.2.8.3 Experimental Factors

794 *Cable Effects*

795 Cable impedances can be analyzed using transmission line methods that invoke an infinite  
796 number of  $\{L, C\}$  components. One line of the cable is considered to be a series of inductances  $L$   
797 and the other line as a zero impedance wire, with capacitances  $C$  connecting the two between  
798 every pair of inductances. In the limit of an infinite number of inductance and capacitance  
799 elements the cable impedance  $Z_{cable} = (L/C)^{1/2}$  is real and constant. Coaxial cables are made so  
800 that  $C$  is 30 pF/ft and  $L$  is 0.075  $\mu H$  / ft so that  $Z_{cable} = (7.5 \times 10^{-8} H / 3.0 \times 10^{-11})^{1/2} = 50 \Omega$ . Thus a  
801 short cable with a 50  $\Omega$  resistor across it looks like an infinitely long cable and a 50  $\Omega$  load on the  
802 cable has an ideal impedance match for maximum power transfer. Such a cable will also behave  
803 as an inductor if short circuited so that for a high conductivity attached sample resonance effects  
804 may be significant.

805

806 *Electrode Polarization*

807 This occurs for two and three terminal measurements when charge transfer does not occur  
808 between an electrode and the sample material, i.e. when the applied voltage is less than the  
809 decomposition potential of the sample (four terminal measurements are immune to this but they  
810 do not produce reliable capacitance data and require separate sample preparation). In this case the  
811 electrode-sample contact can be approximated as a capacitance  $C_s$  in series with the sample [11-  
812 13] that is much larger than the sample capacitance  $C_p$ . If the amplitude of the applied potential is  
813 too large (above the decomposition potential of the electrolyte) a Faradaic impedance [14, 15]  
814 will also occur in parallel with this capacitance [16] that can sometimes be approximated as a  
815 Warburg impedance (see §2.4.3).

816 A series capacitance does not affect  $M''(\omega)$  and simply adds  $1/C_s$  to  $M'(\omega)$ : the total  
817 impedance  $Z_{total}^*(i\omega)$  of the sample impedance  $Z^*(i\omega)$  and  $C_s$  is  $Z_{total}^*(i\omega) = Z^*(i\omega) + 1/i\omega C_s$   
818 so that

819

$$820 \quad M^*(i\omega) = i\omega Z_{total}^* = i\omega Z^*(i\omega) + 1/C_s \quad (2.107)$$

821

822 It is a considerable advantage of the electric modulus function that  $M''(\omega)$  is unaffected by  
823 electrode polarization and other high capacitance phenomena. This is exploited in some of the  
824 methods of data analysis discussed below but it should be noted that some researchers have  
825 correctly noted that  $M^*$  also suppresses low frequency information (relative to  $\varepsilon^*$  for example),  
826 but it can equally be claimed that  $\varepsilon^*$  suppresses high frequency information. The low frequency  
827 high capacitance advantage of  $M^*$  is not shared by the imaginary component of the resistivity  $\rho''$   
828 because

829

$$830 \quad \lim_{\omega \rightarrow 0} \rho''(\omega) \propto \lim_{\omega \rightarrow 0} \left( \frac{1}{k \omega C_s} \right) = \infty, \quad (2.108)$$

831

832 but the low frequency behavior of  $\rho'$  can be useful (see below).

833

834 Electrode polarization can however make the direct determination of the low frequency  
 835 quantities  $\varepsilon_0$  and  $\sigma_0$  difficult and sometimes impossible because it increases  $\varepsilon'$  above  $\varepsilon_0$  at low  
 836 frequencies and, usually at lower frequencies, decreases  $\sigma'$  to below  $\sigma_0$ . Overlap between bulk  
 837 relaxations and these two electrode polarization effects prevents the observation of limiting low  
 838 frequency plateaus in  $\varepsilon'(\omega)$  and/or  $\sigma'(\omega)$ . Although relaxation of electrode polarization often  
 839 occurs at much lower frequencies than the bulk relaxation,

$$840 \quad \tau_{electrode} = \frac{\varepsilon_0 C_s}{C_0 \sigma_0} \gg \frac{\varepsilon_0 C_p}{C_0 \sigma_0} = \tau_D, \quad (2.109)$$

841

842 the magnitude of the polarization dispersion can be very large [proportional to  $(C_s - C_p) \approx C_s$ ]  
 843 and its high frequency tail can extend well into the bulk relaxation region. This phenomenon is  
 844 illustrated by the following representative average circuit quantities: a parallel capacitance  
 845  $C_p = 10$  pF and parallel resistance  $R_p = 10^7$  ohm in series with a polarization capacitance of  
 846  $C_s = 10^4$  pF. Because both  $R_p$  and  $C_p$  will have distributions in a typical electrolyte there will be  
 847 dispersions in both  $\varepsilon'$  and  $\sigma'$  (see §2.4). The dispersion is centered around  
 848  $\omega \approx 1/(R_p C_p) = 10^4$  s<sup>-1</sup> and the low frequency plateau in  $\varepsilon'$  would normally then normally be  
 849 seen at ca.  $\omega \approx 10^2$  s<sup>-1</sup>, but this is dwarfed by the polarization capacitance at that frequency,  
 850  $C_{pol}'(\omega \gg (R_p C_s)^{-1}) = C_s / (\omega^2 R_p^2 C_s^2) = 100$  pF, an order of magnitude higher than  $C_p$ . On the  
 851 other hand, the low frequency dispersion in conductivity due to polarization has barely begun at  
 852  $\omega = 10^2$ :  $\sigma_{ele}' / \sigma_0 = \omega^2 \tau_{ele}^2 / (1 + \omega^2 \tau_{ele}^2) = 0.99$  for  $\omega \tau_{ele} = \omega R_p C_s = (10^2)(10^{-1}) = 10$ , where  
 853 the fact that the limiting high frequency conductivity for the Debye-like relaxation of electrode  
 854 polarization is  $\sigma_0$ :

855

$$856 \quad \lim_{\omega \tau_{ele} \rightarrow \infty} \sigma_{ele}' = \frac{(\varepsilon_0 - \varepsilon_\infty)_{ele} e_0}{\tau_E} = \frac{(\varepsilon_0 - \varepsilon_\infty)_{ele} e_0 \varepsilon_\infty}{\tau_D \varepsilon_0} = \frac{(\varepsilon_0 - \varepsilon_\infty)_{ele} \sigma_0}{\varepsilon_0} \approx \sigma_0 \text{ for } \varepsilon_{0,ele} \gg \varepsilon_{\infty,ele} \quad (2.110)$$

857

858 Effects similar to electrode polarization can arise from other causes, such as poor electrode  
 859 contact where a capacitance due to air gaps occurs in parallel with a resistance at the contact  
 860 areas. Poor contacts have been shown to give spurious dielectric losses in undoped alkali halides  
 861 [17], and is suspected to be responsible for the poor reproducibility of other dielectric data for  
 862 alkali halides [18]. Space charge effects can also produce a series capacitance at the electrode

863 [19,20].

864

### 865 2.3 Dielectric Relaxation

866 An excellent resource for dielectric relaxation is ref. [3], particularly Chapter One by N. E.  
867 Hill. An excellent review of dielectric relaxation phenomena in supercooled and glassy materials  
868 is given by Richert [21] that also includes references to modern measurement techniques.

869

#### 870 2.3.1 Frequency Domain

##### 871 2.3.1.1 Dipole Rotation

872 A freely rotating dipole in a sinusoidally varying electric field with an angular frequency  
873  $\omega$  low enough that the dipole can keep up with the field behaves as a pure capacitance  $C_{pure}$ . The  
874 current then lags the field by  $\pi/2$  radians and the complex admittance is

875

$$876 A^* = i\omega C_{pure}. \quad (2.111)$$

877

878 If the dipole cannot keep up with the field because of friction with its environment it will lag by  
879 an additional angle  $\delta$  and a component of the current appears in phase with the voltage and is  
880 measured as a resistance. Equation (2.94) is then replaced by

881

$$\begin{aligned} 882 I_C &= -V_0\omega C_p \cos(\omega t - \pi/2 - \delta) \\ &= -V_0\omega C_p [\cos(\omega t - \pi/2)\cos\delta + \sin(\omega t - \pi/2)\sin\delta] \\ &= -V_0\omega C_p [\sin(\omega t)\cos\delta - \cos(\omega t)\sin\delta], \end{aligned} \quad (2.112)$$

883

884 and the term  $+V_0\omega C_p \cos(\omega t)\sin\delta$  in eq. (2.112) is seen to be in phase with the applied voltage  
885  $V = +V_0 \cos(\omega t)$ . This in phase component is of course zero when  $\delta = 0$ . Comparing eq. (2.112)  
886 with eqs. (2.95) and (2.96) reveals that

887

$$888 A^* = \omega C_{pure} \sin\delta + i\omega C_{pure} \cos\delta \quad (2.113)$$

889

890 and

891

$$892 C^* = C' - iC'' = C_{pure} \cos\delta - iC_{pure} \sin\delta \quad (2.114)$$

893

894 so that

895

$$896 G_p(\text{effective}) = \omega C_{pure} \sin\delta \quad (2.115)$$

897

898 and

899

$$900 C_p(\text{effective}) = C_{pure} \cos\delta. \quad (2.116)$$

901  
 902 At low frequencies when the lag angle  $\delta$  tends to zero the effective capacitance equals  $C_{pure}$  and  
 903  $G_p = 0$ , as must be. When normalized by the geometric capacitance associated with the cell  
 904 constant  $k$ ,  $C_0 = \epsilon_0 / k$  where  $\epsilon_0$  is the vacuum permittivity  $8.854 \times 10^{-12}$  F m<sup>-1</sup>, the complex  
 905 capacitance becomes the complex permittivity,  $\epsilon^* = C^*/C_0$  so that

$$906 \quad \epsilon^* = \epsilon' - i\epsilon'' \quad (2.117)$$

907  
 908 where

$$909 \quad \epsilon' = \frac{C_p}{C_0} (\epsilon_0 - \epsilon_\infty) \cos(\delta) + \epsilon_\infty, \quad (2.118)$$

$$910 \quad \epsilon'' = \frac{G_p}{\omega \cdot C_0} = \frac{\sigma}{e_0 \cdot \omega} = \frac{C_p}{C_0} (\epsilon_0 - \epsilon_\infty) \sin(\delta), \quad (2.119)$$

911  
 912 and

$$913 \quad \tan \delta = \frac{\epsilon''}{\epsilon'} = \frac{G_p}{\omega C_p}. \quad (2.120)$$

914  
 915 Note that  $\tan \delta$  is independent of the geometric capacitance  $C_0$  and has the same frequency  
 916 dependence as  $\epsilon''$  but with a retardation time of  $(\epsilon_\infty^E / \epsilon_0^E)^{1/2} \tau_E$  rather than  $\tau_E$ . Equations (2.113)  
 917 and (2.114) imply

$$918 \quad A^* = i\omega C_0 \epsilon^* \quad (2.121)$$

919  
 920 so that

$$921 \quad \sigma^* = kA^* = i\omega \epsilon_0 \epsilon^* \quad (2.122)$$

922  
 923 and

$$924 \quad \rho^* = \frac{1}{\sigma^*} = \frac{1}{i\omega \epsilon_0 \epsilon^*} \quad (2.123)$$

925  
 926 The complex electric modulus  $M^*$  is defined as the reciprocal of  $\epsilon^*$ :

$$927 \quad M^* = 1 / \epsilon^* \quad (2.124)$$

928  
 929 so that

937  
938  $M^* = i\omega C_0 Z^* = i\omega e_0 \rho^*$ . (2.125)

939  
940 The functions  $\sigma^*$ ,  $\varepsilon^*$ ,  $\rho^*$  and  $M^*$  are all analytical and their components all conform to the  
941 Cauchy-Riemann and Kronig-Kramers equations. The relationships between them are given in  
942 eq. (2.106).

943 For a single relaxation time the (Debye) functions  $\varepsilon^*(i\omega)$ ,  $\varepsilon'(\omega)$  and  $\varepsilon''(\omega)$  for  
944 dielectric relaxation are  
945

946 
$$\varepsilon^*(i\omega) = \varepsilon_\infty^E + \frac{(\varepsilon_0^E - \varepsilon_\infty^E)}{1 + i\omega\tau_E},$$
 (2.126)

947 
$$\varepsilon'(\omega) = \varepsilon_\infty^E + \frac{(\varepsilon_0^E - \varepsilon_\infty^E)}{1 + \omega^2\tau_E^2},$$
 (2.127)

948  
949 and  
950

951 
$$\varepsilon''(\omega) = \frac{(\varepsilon_0^E - \varepsilon_\infty^E)\omega\tau_E}{1 + \omega^2\tau_E^2},$$
 (2.128)

952  
953 where  $\varepsilon_0^E$  and  $\varepsilon_\infty^E$  are defined in §2.1.1 as the limiting low and high frequency limits of  $\varepsilon'(\omega)$  at  
954 constant electric field, respectively. Equations (2.127) and (2.128) yield a complex plane plot of  
955  $\varepsilon''$  vs  $\varepsilon'$  that is a semicircle centered on the real axis at  $\varepsilon' = (\varepsilon_0^E + \varepsilon_\infty^E)/2$ . This is found by  
956 eliminating  $\omega\tau_E$  between equations (2.127) and (2.128) (see Appendix C in Chapter One for  
957 details).

958 The corresponding Debye functions for  $\sigma'(\omega)$  and  $\sigma''(\omega)$  are

959 
$$\sigma'(\omega) = e_0\omega\varepsilon''(\omega) = \frac{e_0(\varepsilon_0^E - \varepsilon_\infty^E)\omega^2\tau_E}{1 + \omega^2\tau_E^2}$$
 (2.129)

960  
961 and  
962

963 
$$\sigma''(\omega) = e_0\omega\varepsilon_\infty^E + \frac{e_0\omega(\varepsilon_0^E - \varepsilon_\infty^E)}{1 + \omega^2\tau_E^2}.$$
 (2.130)

964  
965 Thus the real part of the conductivity of a Debye dielectric increases from zero at low frequencies  
966 to a high frequency limit of  
967

$$968 \quad \sigma_{\infty} = \lim_{\omega \rightarrow \infty} \sigma'(\omega) = \epsilon_0 (\epsilon_0^E - \epsilon_{\infty}^E) / \tau_E, \quad (2.131)$$

969  
970 and the imaginary part diverges at high frequencies. Derivations of the Debye expressions for  
971  $M'(\omega)$  and  $M''(\omega)$  are instructive and straightforward but tedious – they are given in Appendix  
972 2.1. The results are

$$974 \quad M'(\omega) = M_0^E + \frac{(M_{\infty}^E - M_0^E) \omega^2 \tau_E^2}{1 + \omega^2 \tau_E^2} \quad (2.132)$$

975  
976 and  
977

$$978 \quad M''(\omega) = \frac{(M_{\infty}^E - M_0^E) \omega \tau_E}{1 + \omega^2 \tau_E^2}, \quad (2.133)$$

979  
980 where  $M_0^D = 1 / \epsilon_0^D$ ,  $M_{\infty}^E = 1 / \epsilon_{\infty}^E$ , and  $(\epsilon_{\infty}^E / \epsilon_0^E) \tau_E = \tau_D$ .

981 If a limiting low frequency conductivity  $\sigma_0$  is present that is not physically related to the  
982 dielectric loss process (e.g. ionic conductivity in a dilute aqueous solution), it must be subtracted  
983 from the measured conductivity before the dielectric loss is calculated from eq. (2.128).  
984 Otherwise the limiting low frequency dielectric loss  $\lim_{\omega \rightarrow 0} \epsilon'' \rightarrow 0$  will be masked by the rapid rise  
985 from the conductivity contribution

$$986 \quad \lim_{\omega \rightarrow 0} \epsilon'' = \lim_{\omega \rightarrow 0} \frac{\sigma_0}{\epsilon_0 \omega} \rightarrow \infty. \quad (2.134)$$

988  
989 It has been argued that this subtraction is physically meaningful only if the conductivity is  
990 unrelated to the dielectric loss process (as in the aqueous solutions just mentioned). If the  
991 dielectric loss peak correlates with  $\sigma_0$  as occurs in alkali silicate glasses [22-28] and other  
992 ionically conducting liquids and glasses then the subtraction of  $\sigma_0$  can be regarded as artificial  
993 and other methods of data analysis are preferred (although this position is not universally held).  
994 This is the principle reason for not using the complex permittivity in analyzing highly conducting  
995 materials and is the subject of §2.4.

996 If the decay function is nonexponential then dielectric relaxation can be described in terms  
997 of a distribution of retardation times  $g(\ln \tau_E)$  defined by the relations

$$998 \quad \phi_E(t) = \int_{-\infty}^{+\infty} g(\ln \tau_E) \exp\left(-\frac{t}{\tau_E}\right) d \ln \tau_E \quad (2.135)$$

1000  
1001 and

1002

$$1003 \quad \int_{-\infty}^{+\infty} g(\ln \tau_E) d \ln \tau_E = 1, \quad (2.136)$$

1004

1005 so that eq. (2.126) generalizes to

1006

$$1007 \quad \varepsilon^* - \varepsilon_\infty^E = (\varepsilon_0^E - \varepsilon_\infty^E) \int_{-\infty}^{+\infty} \frac{g(\ln \tau_E)}{1 + i\omega\tau_E} d \ln \tau_E. \quad (2.137)$$

1008

1009 The generalization of eqs. (2.127) and (2.128) are

1010

$$1011 \quad \varepsilon'(\omega) = \varepsilon_\infty^E + (\varepsilon_0^E - \varepsilon_\infty^E) \left[ \int_{-\infty}^{\bar{\quad}} g(\ln \tau_E) \frac{1}{1 + \omega^2 \tau_E^2} d \ln \tau_E \right] = \varepsilon_\infty^E + (\varepsilon_0^E - \varepsilon_\infty^E) \left\langle \frac{\omega\tau_E}{1 + \omega^2 \tau_E^2} \right\rangle \quad (2.138)$$

1012

1013 and

1014

$$1015 \quad \varepsilon''(\omega) = (\varepsilon_0^E - \varepsilon_\infty^E) \int_{-\infty}^{\bar{\quad}} g(\ln \tau_E) \frac{\omega\tau_E}{1 + \omega^2 \tau_E^2} d \ln \tau_E = (\varepsilon_0^E - \varepsilon_\infty^E) \left\langle \frac{\omega\tau_E}{1 + \omega^2 \tau_E^2} \right\rangle. \quad (2.139)$$

1016

1017 The  $n^{\text{th}}$  moments of a distribution function are

1018

$$1019 \quad \langle \tau_E^n \rangle = \int_{-\infty}^{+\infty} \tau_E^n g(\ln \tau_E) d \ln \tau_E. \quad (2.140)$$

1020

1021 If the integral  $\int_{-\infty}^{+\infty} g(\ln \tau_E) d \ln \tau_E$  diverges, as it does for a constant phase angle impedance for

1022 example,  $g(\ln \tau_E)$  is not renormalizable and a constant phase angle impedance can therefore be

1023 valid only over a limited range in relaxation times. In terms of  $\phi(t)$  the moments are

1024

$$1025 \quad \langle \tau_E^n \rangle = \frac{1}{\Gamma(\omega)} \int_0^{+\infty} t^{n-1} \phi(t) dt \quad (2.141)$$

1026

1027 and

1028

$$1029 \quad \langle \tau_E^{-n} \rangle = (-1)^n \left[ \frac{d^n(\phi_E)}{dt^n} \right]_{t=0} \quad (2.142)$$

1030

## 1031 2.3.1.2 Ionic Hopping

1032 Chapter One of [3] by N. E. Hill discusses the studies of Frohlich [6] and others on the  
 1033 dielectric relaxation consequences of two state models. We select here the Frohlich account of an  
 1034 entity that has only two possible equilibrium positions 1 and 2. The entity could be a molecular  
 1035 dipole or an ion for example. If the transition probabilities between the two positions are  $w_{12}$  and  
 1036  $w_{21}$  when there is no applied field then a Debye relaxation with a single relaxation time  
 1037  $\tau_E = 1/(w_{12} + w_{21})$  is predicted that has an Arrhenius temperature dependence  
 1038  $\tau_E = A_E \exp(\Delta H / RT)$  where the pre-exponential factor  $A_E$  is a weak function of temperature and  
 1039  $\Delta H$  is the energy barrier that separates the two positions. As noted by Hill, however, a  
 1040 nonexponential decay function may result from local field effects.

1041

## 1042 2.3.2 Resonance Absorption

1043 The resonance expression for  $\varepsilon^*(i\omega)$  is given by eq. 1.395 in Chapter One, repeated here  
 1044 for convenience:

1045

$$1046 \quad \varepsilon^*(i\omega) = \frac{\omega_0^2 - \omega^2 + i\omega\gamma}{(\omega_0^2 - \omega^2)^2 + \omega^2\gamma^2}. \quad (2.143)$$

1047

1048 The corresponding expression for the real component of the conductivity is

1049

$$1050 \quad \sigma'(\omega) = e_0\omega\varepsilon''(\omega) = \frac{e_0\omega^2\gamma}{(\omega_0^2 - \omega^2)^2 + \omega^2\gamma^2}. \quad (2.144)$$

1051

1052 For  $\omega \ll \omega_0$ , appropriate for almost all relaxation processes, eq. (2.144) becomes

1053

$$1054 \quad \lim_{\omega \ll \omega_0} \sigma'(\omega) = \frac{e_0\omega^2\gamma}{\omega_0^4}, \quad (2.145)$$

1055

1056 so that  $\sigma'(\omega)$  is proportional to  $\omega^2$ . Since the strongest frequency dependence of conductivity  
 1057 for relaxation processes is  $\omega$  power law exponents greater than unity imply a resonance process  
 1058 at high frequencies.

1059

## 1060 2.3.3 Time Domain

1061 Consider the case where an electric field  $E$  is "instantaneously" increased from zero to  $E_0$   
 1062 across a dielectric sample at time  $t = t'$  and kept constant thereafter, i.e.  $E(t) = E_0 h(t - t')$  where  
 1063  $h(t)$  is the Heaviside function (eq. (1.327)). The initially randomized dipoles will partially orient  
 1064 themselves over time and the polarization and displacement will both increase (the final average  
 1065 orientation will not be complete because of thermal fluctuations):

1066

$$1067 \quad D(t) = D(0) + [D(\infty) - D(0)][1 - \phi_E(t)], \quad (2.146)$$

1068  
 1069 where  $D(0)$  and  $D(\infty)$  are the limiting short time (high frequency) and long time (low  
 1070 frequency) values of  $D(t)$  and  $\phi_E(t)$  is the decay function for polarization at constant  $E$   
 1071 corresponding to  $D(t)$ . The increase of  $D$  from zero to  $D(\infty)$  is "instantaneous" compared with  
 1072 dielectric relaxation times (generally no shorter than about  $10^{-11}$  s) and is due to polarization of  
 1073 molecular electron clouds that occurs roughly on optical time scales.

1074 It is sometimes convenient to approximate the relation between time domain data and  
 1075  $\varepsilon''(\omega)$  by the Hamon approximation

1076  
 1077 
$$\varepsilon''(\omega) \approx (\varepsilon_0^E - \varepsilon_\infty^E) \left( \frac{-d\phi_E}{dt} \right) \left( \frac{5t}{\pi} \right), \quad (2.147)$$

1078  
 1079 obtained from the simplification that the normalized displacement current is given by

1080  
 1081 
$$\left( \frac{-d\phi_E}{dt} \right) \sim t^{-n}. \quad (2.148)$$

1082  
 1083 No comparably simple relation exists between  $\varepsilon'(\omega)$  and  $\phi(t)$ . Williams, Watt, Dev and North  
 1084 [29] have shown that for the Williams-Watt [30] decay function

1085  
 1086 
$$\phi(t) = \exp \left[ - \left( \frac{t}{\tau_0} \right)^\beta \right] \quad (2.149)$$

1087  
 1088 the Hamon approximation is accurate within 1% for  $\omega\tau_0 > 1$  but fails for  $\omega\tau_0 \leq 1$  and  $\beta > 0.2$ .  
 1089 Equation (2.147) therefore offers a high frequency approximation to the broadest frequency  
 1090 domain Williams-Watt functions that cannot be expressed in terms of named functions.

1091 The complex relative permittivity  $\varepsilon^*(\omega)$  is related to the derivative of  $\varepsilon(t)$  by

1092  
 1093 
$$\varepsilon^*(i\omega) - \varepsilon_\infty^E = (\varepsilon_0^E - \varepsilon_\infty^E) \int_0^\infty \left( \frac{d\phi_E}{dt} \right) \exp(-i\omega t) dt \quad (2.150)$$

1094  
 1095 where  $\varepsilon_0^E = D(\infty)/E_0$  and  $\varepsilon_\infty^E = D(0)/E_0$ . In the simplest case  $\phi_E(t)$  is exponential,

1096  
 1097 
$$\phi_E(t) = \exp \left[ - \left( \frac{t}{\tau_E} \right) \right], \quad (2.151)$$

1098

.....

1099 and insertion of eq. (2.151) into eq. (2.150) yields the Debye equations (2.127) and (2.128)  
 1100 [Chapter One of ref. 3].

#### 1101 1102 2.3.4 Temperature Domain

1103 In many situations  $\omega$  and  $\tau_E$  are approximately interchangeable variables. Since  $\tau_E$  often  
 1104 varies strongly with temperature a narrow temperature range can be used as a surrogate for a wide  
 1105 frequency range. The temperature dependence of  $\tau_E$  is often approximated by the Arrhenius  
 1106 relation

$$1108 \quad \tau = \tau_0 \exp\left(\frac{E_a}{RT}\right), \quad (2.152)$$

1109 where  $\tau_0$  is independent of temperature, R is the ideal gas constant, and  $E_a$  is the activation  
 1110 energy. A better approximation is the Fulcher equation

$$1113 \quad \tau_E = A_F \exp\left(\frac{B_F}{T - T_0}\right) \quad (2.153)$$

1114 where  $A_F$ ,  $B_F$  and  $T_0$  are positive constants. Thus the variables  $\ln(\omega\tau)$  at constant  $\omega$ , and  $E_a/RT$   
 1115 or  $B_F/(T - T_0)$ , are equivalent for a single relaxation time dielectric. In this case eqs. (2.152) and  
 1116 (2.153) indicate that over the convenient temperature range from liquid nitrogen (77 K) to room  
 1117 temperature (300K) the retardation time can vary over a very large range. For example  $\tau$  changes  
 1118 by a factor of  $10^{25}$  for an average activation energy of 50 kJ/mol. The temperature variable is  
 1119 therefore extremely useful for scans of the total relaxation spectrum and is frequently used for  
 1120 polymers whose relaxation behavior is typically characterized by widely separated and broad  
 1121 relaxation processes. Activation energies  $E_a$  are obtained from plots of log frequency  $\ln f$  against  
 1122 the inverse temperature  $1/T_{\max}$  at which  $\varepsilon''$  or  $\tan \delta$  passes through its maximum:

$$1125 \quad \left\langle \frac{E_a}{R} \right\rangle = - \left[ \frac{d \ln f}{d(1/T)} \right]. \quad (2.154)$$

1126 It has been reported [32] that the activation energy obtained in this way is ambiguous because it  
 1127 depends on whether the derivative is determined in the isothermal frequency domain or in the  
 1128 temperature domain at constant frequency: the frequency domain plot of  $\ln f_{\max}$  vs.  $1/T$  was found  
 1129 to be strongly curved whereas the plot of  $\ln f$  vs.  $1/T_{\max}$  was found to be linear.

1131 Although temperature is useful because of its experimental convenience it is not  
 1132 quantitative because "everything changes with temperature". For example the dispersion  
 1133  $(\varepsilon_0^E - \varepsilon_\infty^E)$  can only be estimated because  $\varepsilon_0^E$  and to a less extent  $\varepsilon_\infty^E$  are temperature dependent,  
 1134 although it can be estimated from the relation [33]

1135

$$1136 \quad (\varepsilon_0^E - \varepsilon_\infty^E) \approx \left( \frac{2}{\pi R} \right) \left\langle \frac{1}{E_A} \right\rangle^{-1} \int_0^\infty \varepsilon''(T) d(1/T). \quad (2.155)$$

1137  
 1138 Equation (2.155) is an approximation because of two assumptions in its derivation that must be  
 1139 made for mathematical tractability: (i)  $(\varepsilon_0^E - \varepsilon_\infty^E)$  is independent of temperature [32] and (ii)  
 1140  $\langle E_a \rangle = \langle 1/E_a \rangle^{-1}$  (not generally true because of the Schwarz inequality eq. 1.333):.

$$1141 \quad \langle E_A \rangle \langle 1/E_A \rangle^{-1} \geq 1. \quad (2.156)$$

1142  
 1143 There are two situations where  $\ln \omega$  and  $E_a/RT$  are not even approximately equivalent:  
 1144 (i) functions for which  $\omega$  and  $\tau_E$  are not invariably multiplied together (for example the  
 1145 conductivity of a Debye dielectric, eq. (2.128));  
 1146 (ii) distributions of retardation times that change with temperature.

### 1147 2.3.5 Equivalent Circuits

1148 The electrical response for an exponential dielectric decay function, the Debye relations  
 1149 eqs. (2.127) and (2.128) plus any separate conductivity contribution  $\sigma_0$ , is simulated by an  
 1150 equivalent circuit comprising three parallel arms: a capacitance  $C_p$ , a series combination of  $R_s$   
 1151 and  $C_s$ , and a resistance  $R_p$ . The relaxation part of the circuit is the series component  $R_s + C_s$ ,  
 1152 the parallel resistance  $R_p$  corresponds to the separate conductivity, and the parallel capacitance  
 1153  $C_p$  simulates the limiting high frequency permittivity. If for a particular range of frequencies the  
 1154 equivalent circuit of an experimental sample resembles  $R_s + C_s$  and the frequency range  
 1155 encompasses  $\omega = 1/(R_s C_s)$  then a dielectric loss peak will be observed in that frequency range. An  
 1156 example is electrode polarization in a conducting medium that at low frequencies is approximated  
 1157 by an electrode capacitance in series with the low frequency resistance of the sample. In this case  
 1158 a dielectric loss is observed with a retardation time given by the product of the polarization  
 1159 capacitance and sample resistance. Electrode polarization effects in solid electrolytes can often be  
 1160 a serious problem; they were briefly discussed in §2.2.8.3 and are discussed in detail in §2.3.6.1  
 1161 and §2.3.6.4 below.

1162 In terms of the equivalent circuit the components of the complex permittivity are (see  
 1163 Appendix 2.3)

$$1164 \quad \varepsilon'(\omega) = \frac{\sigma''}{\varepsilon_0 \omega} = \left( \frac{1}{C_0} \right) \left( C_p + \frac{C_s}{1 + \omega^2 \tau_E^2} \right) \quad (2.157)$$

1165 and  
 1166  
 1167  
 1168  
 1169  
 1170

$$1171 \quad \varepsilon''(\omega) = \frac{\sigma'}{e_0\omega} = \left(\frac{C_s}{C_0}\right) \left(\frac{\omega\tau_E}{1+\omega^2\tau_E^2}\right) + \frac{\sigma_0}{e_0\omega}, \quad (2.158)$$

1172  
1173 that reproduce the Debye relations eqs. (2.127) and (2.128). The low and high frequency limits of  
1174  $\varepsilon'$  are

$$1176 \quad \lim_{\omega \rightarrow 0} \varepsilon'(\omega) = \varepsilon_0 = \left(\frac{C_p + C_s}{C_0}\right) \quad (2.159)$$

1177  
1178 and  
1179

$$1180 \quad \lim_{\omega \rightarrow \infty} \varepsilon'(\omega) = \varepsilon_\infty = \left(\frac{C_p}{C_0}\right). \quad (2.160)$$

1181  
1182 Matlab®/GNUOctave codes for computing  $M^*(i\omega)$  and  $\rho^*(i\omega)$  with the added  $R_p$  are given in  
1183 Appendix 2.2. A notable result is that  $M^*(i\omega)$  exhibits two relaxations corresponding to the  
1184 Debye relaxation and an additional relaxation due to  $\sigma_0$ . The Debye relaxation for  $M^*(i\omega)$  is  
1185 unaffected by  $R_p$  but the conductivity relaxation due to  $\sigma_0$  is.

1186 As noted in §2.1 the occurrence of a dielectric and conductivity relaxation together raises  
1187 an important nomenclature issue that has produced much confusion: the subscripts for denoting  
1188 limiting low and high frequency limits can be ambiguous because these limits can refer to either  
1189 the average dielectric relaxation frequency or to the average conductivity relaxation frequency. In  
1190 particular, the quantity  $\varepsilon_\infty$  that enters into the expression for the conductivity relaxation time,  
1191  $\langle\tau_D\rangle = e_0\varepsilon_\infty / \sigma_0$ , is the high frequency limit for the conductivity relaxation, that may correspond  
1192 to the low frequency limit for a separate dielectric relaxation. A proposed nomenclature to resolve  
1193 this ambiguity was given above in §2.1 and has already been used in this section.

### 1194 1195 2.3.6 Interfacial Polarization

1196 In a homogeneous material  $\vec{\nabla} \cdot \vec{\mathbf{D}} = e_0\varepsilon \vec{\nabla} \cdot \vec{\mathbf{E}} = 0$  implies  $\vec{\nabla} \cdot \vec{\mathbf{E}} = 0$ . At the interface between  
1197 two dielectric materials of different permittivity, however, there is a discontinuity in  $\varepsilon$  and  
1198  $\vec{\nabla} \cdot \vec{\mathbf{D}} = 0$  no longer implies  $\vec{\nabla} \cdot \vec{\mathbf{E}} = 0$ . The solution to this problem is obtained by applying  
1199 Gauss's and Stokes' theorems to the interface with the result that the component of  $\vec{\mathbf{E}}$  tangential  
1200 to the interface is continuous across the interface and the normal component of  $\vec{\mathbf{D}}$  is either  
1201 continuous (no interfacial charge) or discontinuous if there is a free charge that is not the result of  
1202 polarization of the materials on each side of the interface. These boundary conditions make  
1203 macroscopic interfacial effects dependent on the geometry of the interface.

1204 Relaxation of interfacial polarization between alternating slabs of insulating dielectric and  
1205 conducting layers, generically referred to as a Maxwell Layered Dielectric, is characterized by a  
1206 single relaxation time  $\tau_i$  given by

1207

$$1208 \quad \tau_i = R_s C_s = \left( \frac{\ell_R}{\ell_C} \right) \epsilon_0 \rho \epsilon = \left( \frac{\ell_R}{\ell_C} \right) \left( \frac{\epsilon_0 \epsilon}{\sigma} \right) \quad (2.161)$$

1209

1210 where  $\ell_R$  is the thickness of the resistive layer with material resistivity  $\rho$  and  $\ell_C$  is the thickness  
1211 of the capacitive layer with material permittivity  $\epsilon$ .

1212

### 1213 2.3.7 Maxwell-Wagner Polarization

1214 Relaxation of interfacial polarization between a conducting sphere embedded in a  
1215 dielectric continuum is known as Maxwell-Wagner (MW) polarization. Wagner [34] computed  
1216 the loss tangent ( $\tan \delta$ ) for a volume fraction  $\phi$  of spheres of material conductivity  $\sigma_1$  and  
1217 relative permittivity  $\epsilon_1$  suspended in a dielectric medium of relative permittivity  $\epsilon_2$ , that was then  
1218 generalized by Sillars [35] to suspensions of nonspherical particles. An excellent discussion of the  
1219 phenomenon is given in ref [3] from which much of the following is distilled. We also draw from  
1220 the paper by van Beek [36] who gave the Sillars formula and then considered the special case of  
1221 suspended spheres, and noted that the often cited Wagner formula is only correct when the  
1222 permittivities of the suspended material and the dielectric medium are equal and that the Sillars  
1223 expression does not have this flaw.

1224 The Sillars expression for aspherical particles with aspect ratio  $a/b$  and  $a$  parallel to the  
1225 field direction is

1226

$$1227 \quad \tan \delta = \frac{\epsilon_2 K}{\left[ \epsilon_\infty (\epsilon_2 K + \epsilon_\infty) \right]^{1/2}} \left( \frac{\omega \tau_0}{1 + \omega^2 \tau_0^2} \right), \quad (2.162)$$

1228

1229 with

1230

$$K = \frac{n^2 \phi \epsilon_2}{\left[ (n-1) \epsilon_2 + \epsilon_1 \right]} \quad (a),$$

$$\epsilon_\infty = \epsilon_2 \left[ 1 + \frac{n \phi (\epsilon_2 - \epsilon_1)}{(n-1) \epsilon_2 + \epsilon_1} \right] \quad (b),$$

1231

$$T = \frac{\epsilon_0 \left[ (n-1) \epsilon_2 + \epsilon_1 \right]}{\sigma_1} \quad (c),$$

$$\tau_0 = \frac{T}{\left\{ (\epsilon_1 K + \epsilon_\infty) / \epsilon_\infty \right\}^{1/2}} \quad (d),$$

1232

1233 where  $n$  is a function of the aspect ratio  $a/b$ . The limiting values for  $n$  are

1234

$$\begin{aligned}
1235 \quad n &\sim 1 && (a < b) && (a) \\
n &= 3 && (a = b) && (b) \\
n &\approx \left\{ \frac{a^2}{b^2 [\ln(2a/b) - 1]} \right\} && (a > b) && (c),
\end{aligned} \tag{2.164}$$

1236  
1237 Equation (2.164)(c) indicates that for needle-like particles oriented in the direction of the field the  
1238 value of  $n$  can be large – for example  $n \sim 50$  for  $a = 10b$ . Because  $\tan \delta$  is roughly proportional to  
1239  $n^2$  [eqs. (2.162) and (2.163)a] the Maxwell-Wagner-Sillars effect can produce very large dielectric  
1240 losses. For spherical particles  
1241

$$\begin{aligned}
1242 \quad K &= \frac{9\phi\epsilon_2}{[2\epsilon_2 + \epsilon_1]} && (a), \\
e_\infty &= \epsilon_2 \left[ 1 + \frac{3\phi(\epsilon_2 - \epsilon_1)}{2\epsilon_2 + \epsilon_1} \right] && (b), \\
T &= \frac{e_0 [2\epsilon_2 + \epsilon_1]}{\sigma_1} && (c),
\end{aligned} \tag{2.165}$$

1243  
1244 and  $\tau_0$  is again given by eq. (2.163)d. The maximum value of  $\tan \delta$  computed from eq. (2.162)d  
1245 is therefore  
1246

$$1247 \quad \tan \delta_{\max} = \frac{\epsilon_2 K}{2[e_\infty(\epsilon_2 K + e_\infty)]^{1/2}}. \tag{2.166}$$

1248  
1249 This expression is inconveniently complicated but simplifies when  $\phi \rightarrow 0$ :  
1250

$$1251 \quad \lim_{\phi \rightarrow 0} (\tan \delta_{\max}) = \frac{9\phi\epsilon_2}{2(2\epsilon_2 + \epsilon_1)}. \tag{2.167}$$

1252  
1253 The components of the complex relative permittivity for the Maxwell-Wagner phenomenon for  
1254 this limiting case are conveniently expressed using three ancillary functions [36]:  
1255

$$1256 \quad \epsilon_\phi = \epsilon_2 \left\{ 1 + \frac{3\phi(\epsilon_1 - \epsilon_2)}{2\epsilon_2 + \epsilon_1} \right\}, \tag{2.168}$$

$$1257 \quad S = \frac{9\phi\epsilon_2}{2\epsilon_2 + \epsilon_1}, \tag{2.169}$$

1259

$$1260 \quad T = \frac{\sigma_1}{e_0(2\varepsilon_2 + \varepsilon_1)}. \quad (2.170)$$

1261

1262 Then

1263

$$1264 \quad \varepsilon'' = \frac{(\varepsilon_\phi S \omega T)}{1 + \omega^2 T^2} \quad (2.171)$$

1265

1266 and

1267

$$1268 \quad \varepsilon' = \varepsilon_\phi \left\{ 1 + \frac{S}{1 + \omega^2 T^2} \right\}. \quad (2.172)$$

1269

1270 The maximum in the observed dielectric loss  $\varepsilon''_{MW}$  is therefore

1271

$$1272 \quad \varepsilon''_{\max} = \frac{9\phi\varepsilon_2^2}{2(2\varepsilon_2 + \varepsilon_1)} \left[ 1 + \frac{3\phi(\varepsilon_2 - \varepsilon_1)}{2\varepsilon_{12} + \varepsilon_1} \right] \rightarrow \frac{9\phi\varepsilon_2^2}{2(2\varepsilon_2 + \varepsilon_1)}, \quad (2.173)$$

1273

1274 that occurs at an angular frequency  $\omega_{\max}$  given by

1275

$$1276 \quad \omega_{\max} = 1/\tau_{MW} = \frac{\sigma_1}{e_0(2\varepsilon_1 + \varepsilon_2)}. \quad (2.174)$$

1277

1278 At  $\omega_{\max}$  the value of  $\varepsilon'$  from eq. (2.172) is  $\lim_{\phi \rightarrow 0} \varepsilon' = \varepsilon_2$  that when combined with eq. (2.173)

1279 produces eq. (2.167).

1280

1281 

### 2.3.8 Examples

1282 Attention is restricted to the dielectric relaxation of water molecules in different  
1283 environments.

1284

1285 

#### 2.3.8.1 Liquid Water

1286 Water is one of the few liquids that relaxes with a single retardation time (or very close to  
1287 it) and therefore has a Debye complex permittivity. Its dielectric relaxation frequency depends on  
1288 temperature but always lies within the microwave region of the em spectrum. This has important  
1289 implications for both navigational and meteorological radar and is of course the basis for  
1290 microwave cooking. The temperature dependence of the retardation time is not Arrhenius but  
1291 rather adheres to the empirical Fulcher equation (1.543) and (2.153), repeated here for  
1292 convenience:

1293

$$1294 \quad \tau = A_F \exp\left(\frac{B_F}{T - T_0}\right), \quad (2.175)$$

1295

1296 with parameters  $A_F = 1.25 \times 10^{-13}$  s,  $B_F = 669$  K,  $T_0 = 138$  K that give a good description of  $\tau(T)$

1297 down to the limit of supercooling of bulk water, ca.  $-35^\circ\text{C}$ . The relaxation frequency  $(1/2\pi\tau)$

1298 therefore varies between 62 GHz at  $0^\circ\text{C}$  and 74 GHz at  $100^\circ\text{C}$  and the energy absorption at  $100^\circ\text{C}$

1299 is about 75% that at  $0^\circ\text{C}$ . Microwave ovens generally operate at a frequency 2.45 GHz that

1300 lies on the low frequency side of the Debye dielectric loss peak - the dielectric losses at this

1301 frequency are about 4.0% and 3.3% of the maximum loss. The fact that the frequency of a

1302 microwave oven is on the lower side of the dielectric loss peak of water means that energy

1303 absorption decreases with increasing temperature as the loss peak moves to higher frequencies,

1304 thus preventing runaway heating.

1305

### 1306 2.3.8.2 Supercooled Water

1307 Maxwell-Wagner polarization has been used to obtain the relative permittivity of

1308 supercooled water down to about  $-35^\circ\text{C}$  [37, 38]. The Maxwell-Wagner losses occur in the

1309 frequency range  $10^5 - 10^6$  Hz that is far below the frequency range for the dielectric relaxation of

1310 water (around  $10^{11}$  Hz) so that the measured values for the relative permittivity correspond to the

1311 limiting low frequency value  $\epsilon_0 > \sim 80$ . This range is also far above the relaxation frequency for

1312 ice that is about  $10^{3.5}$  Hz at  $0^\circ\text{C}$  and decreases with decreasing temperature, so that if

1313 crystallization occurred the relevant relative permittivity of ice is the limiting high frequency

1314 value  $\epsilon_\infty \sim 5$ , far smaller than the limiting low frequency value  $\epsilon_0 > \sim 80$ . It is fortunate that the

1315 Maxwell-Wagner losses occur at frequencies between the relaxation frequency ranges of water

1316 and ice and do not overlap with either.

1317 Emulsions of water in heptane stabilized by the surfactant sorbitol tristearate [37] and

1318 droplets suspended in beeswax [38] both exhibit Maxwell-Wagner polarization. In the first and

1319 rigorous beeswax study by Hasted and Shahidi [38] volume fractions of 0.5% and 1.0% were

1320 used. Hodge and Angell [37] later used a much larger volume fraction of water (30%) that was

1321 necessitated by their much lower instrumental sensitivity. Their data were stated to be

1322 inconsistent with the Maxwell-Wagner formulae because the observed values of  $\epsilon''_{\text{max}}$  were

1323 claimed to be about four times larger than predicted and their sign of  $(d\epsilon''_{\text{max}}/dT) \propto (d\epsilon_1/dT)$  was

1324 positive rather than negative as predicted by their eq. (3). However their eq. (3) is incorrect - the

1325 numerator term  $\epsilon_2^2$  of eq. (2.173) was given as  $\epsilon_1^2$  so that the analyses of  $\epsilon''_{MW}$  given in [1] and

1326 [37] are both incorrect. Equation (2.173) predicts that  $\epsilon''_{\text{max}}$  is indeed inversely proportional to  $\epsilon_1$

1327 if  $\epsilon_1 \gg \epsilon_2$  (a good approximation for water droplets in hexane). The analyses in terms of the

1328 electric modulus [1,37] are unaffected by this mistake and remain valid although the stated

1329 requirement that a series capacitance that simulates the surfactant layer around the droplet needs

1330 to be large for the modulus analysis to be useful [1] is not correct (see eq. (2.107) above).

1331 The observed maxima in  $\epsilon''$  decreased with decreasing temperature that is consistent with

1332 eq. (2.173), but for  $\varepsilon_1 \approx 100 \gg \varepsilon_2 \approx 2$  and  $\phi = 0.3$  the predicted value is about  
 1333  $\varepsilon''_{\max} \approx \{(9)(0.3)(4)/[2(106)]\} \approx 0.005$ , compared with the experimental values that range  
 1334 between about 0.4 – 0.8. The observed value is therefore too large by a factor of about 100. Also,  
 1335 the measured ratio of  $\varepsilon''_{\max}$  at the temperature extremes of 0°C and -35°C is about 1.8 compared  
 1336 with the correct value of about 1.2. The observed values of  $\omega_{\max}$  for  $\varepsilon''$  were centered  
 1337 around  $2\pi(5.5 \times 10^6 \text{ Hz}) \approx 3.5 \times 10^7 \text{ rad/s}$  from which eq. (2.174) predicts a conductivity of about  
 1338  $\sigma_1 \approx \varepsilon_0 [(2\varepsilon_1 + \varepsilon_2) + \phi(\varepsilon_1 - \varepsilon_2)] \omega_{\max} / (1 - \phi) \approx (9 \times 10^{-12} \text{ F/m})(230)(3.5 \times 10^7) / 0.7$   
 1339  $\approx (9 \times 10^{-12} \text{ F/m})(230)(3.5 \times 10^7) / 0.7 \approx 0.1 \text{ S/m}$ , that is impossibly high.

1340 The measured modulus peak heights also decreased with decreasing temperature and since  
 1341  $M''_{\max}$  is assumed to be inversely proportional to the permittivity this trend is also in the correct  
 1342 direction. Values of  $\varepsilon_1$  for water were then derived by assuming that  $M''_{\max} \propto 1/\varepsilon_1$ , fixing the  
 1343 proportionality constant from literature data for  $\varepsilon_1$  at 0 °C and then least squares fitting a  
 1344 quadratic in temperature to eight data points between 0°C and -35 °C. Agreement with the earlier  
 1345 results, of which the authors were unaware at the time of paper submission (see Note added in  
 1346 Proof in [37]), was within the  $\pm 2\%$  uncertainties claimed for each method but the agreement is  
 1347 better than this because most of the discrepancies are systematic due to the different values of  $\varepsilon_1$   
 1348 at 0°C for the two methods (measured in [38] but chosen from the literature as a proportionality  
 1349 constant in [37]). When this is corrected for by equating the average of the modulus derived  
 1350 permittivities to the average from reference [38] the differences are reduced to 0.5% or less. This  
 1351 is a remarkable result given the simplifications used in the modulus analysis.

1352 These Maxwell-Wagner results can be rationalized in terms of a simplified equivalent  
 1353 circuit for the emulsified water droplets: a parallel ( $R_1 C_1$ ) element (corresponding to the water  
 1354 droplet with relative permittivity  $\varepsilon_1$  and conductivity  $\sigma_1$ ) is in series with a capacitance  $C_s$  that  
 1355 simulates the suspected thin layer of emulsifier, and a capacitance  $C_2$  in parallel with the series  
 1356 combination to simulate the surrounding heptane. Intuitively  $C_2$  is much smaller than  $C_1$  from  
 1357 both geometrical and physical considerations ( $\varepsilon_2 \ll \varepsilon_1$ ). The circuit analysis is:

1358 (i) Admittance  $A_1$  of parallel ( $R_1 C_1$ ) element:

$$1359 \quad A_1 = 1/R_1 + i\omega C_1 = (1 + i\omega R_1 C_1) / R_1 = (1 + i\omega \tau_1) / R_1 \text{ so that}$$

$$1360 \quad Z_1 = R_1 / (1 + i\omega \tau_1). \quad (2.176)$$

$$1361 \quad (ii) \quad \text{Impedance of } \{(R_1 C_1) + C_s\} \text{ arm} = Z_{1s} = \frac{R_1}{1 + i\omega \tau_1} + \frac{1}{i\omega C_s} = \frac{i\omega R_1 C_s + 1 + i\omega \tau_1}{i\omega C_s (1 + i\omega \tau_1)} \Rightarrow$$

$$1362 \quad A_{1s} = \frac{i\omega C_s (1 + i\omega \tau_1)}{1 + i\omega (\tau_1 + R_1 C_s)}. \quad (2.177)$$

1366

1367 (iii) Admittance  $A_{1s2}$  of complete circuit:

$$1368 \quad A_{1s2} = A_{1s} + i\omega C_2 = \frac{i\omega C_s - \omega^2 C_s \tau_1 + i\omega C_2 [1 + i\omega(\tau_1 + R_1 C_s)]}{1 + i\omega(\tau_1 + R_1 C_s)} =$$

$$1369$$

$$1370 \quad \frac{i\omega(C_s + C_2) - \omega^2(C_s \tau_1 + C_2 \tau_1 - R_1 C_s C_2)}{1 + i\omega(\tau_1 + R_1 C_s)}. \quad (2.178)$$

1371 (iv) For  $C_2 \ll C_1$  appropriate for water droplets in heptane the total admittance simplifies to

$$1374 \quad A_{1s2} = \frac{i\omega C_s - \omega^2 R_1 C_1 C_s}{1 + i\omega R_1 (C_1 + C_s)}. \quad (2.179)$$

1375 Thus

$$1378 \quad C_{1s2}^* = \frac{A_{1s2}}{i\omega} = \frac{C_s (1 + i\omega R_1 C_1)}{1 + i\omega R_1 C_s} = \frac{C_s (1 + i\omega R_1 C_1)(1 + i\omega R_1 C_s)}{1 + \omega^2 R_1^2 C_s^2}$$

$$= \frac{C_s - \omega^2 R_1^2 C_1 C_s}{1 + \omega^2 R_1^2 C_s^2} + \frac{i\omega C_s R_1 (C_1 + C_s)}{1 + \omega^2 R_1^2 C_s^2}.$$

1379 so that

$$1382 \quad C'' = \frac{\omega C_s R_1 (C_1 + C_s)}{1 + \omega^2 R_1^2 C_s^2}. \quad (2.181)$$

1383 The maximum value  $(C_1 + C_s)/2$  for  $C''$  is therefore determined in part by the surfactant layer  
 1384 and is greater than the value  $C_1/2$  for no series capacitance. This is consistent with the observed  
 1385 maxima in  $\epsilon''$  [37] being about 100 times greater than that calculated from the Maxwell-Wagner  
 1386 expression. The maximum in  $C''$  also occurs at  $\omega_{\max} = 1/(R_1 C_s)$  that is also determined in part by  
 1387 the surfactant layer and therefore would give an incorrect value for the conductivity of water. This  
 1388 dependency of the relaxation time on  $C_s$  can also account for the (unreported) fact that changing  
 1389 the suspending medium changed  $\omega_{\max}$  [37] since the suspending medium would be expected to  
 1390 affect the surfactant layer and  $C_s$ .

1392 The imaginary component of the electric modulus for the same circuit when  $C_2 \ll C_1$  is

$$1394 \quad M'' = \frac{i\omega R_1}{(1 + i\omega^2 R_1^2 C_1^2)} = \left( \frac{1}{C_1} \right) \frac{i\omega R_1 C_1}{(1 + i\omega^2 R_1^2 C_1^2)}, \quad (2.182)$$

1395

1396 the maximum value of which is  $1/(2C_1)$  and therefore contains the desired information about  $C_1$   
 1397 that is independent of  $C_s$ . The frequency of maximum  $M''$  is  $\omega_{\max} = 1/(R_1C_1)$  and is also  
 1398 independent of  $C_s$ .

1399 Matlab® and GNUOctave calculations of the relaxation functions for the circuit enable  
 1400 values of the circuit elements to be quickly estimated that produce trends that are generally  
 1401 consistent with the experimental data, with the notable exception of the maximum values of  $\epsilon''$   
 1402 (discussed briefly below). For example good agreement with the experimental trends is attained  
 1403 with  $R_1 = 10^3 \Omega$ ;  $C_1 = 10^{-3} \text{ F}$ ;  $C_2 = 10^{-5} \text{ F}$ ;  $C_s = 5 \times 10^{-4} \text{ F}$ . The value of 100 for the ratio  $C_1/C_2$   
 1404 was chosen to approximate the ratio of permittivities of water and hexane and to accommodate an  
 1405 unknown geometric factor for the suspending medium relative to the droplet, and the value of  $C_s$   
 1406 was found from the experimental ratio of 0.5 for the frequencies of maximum  $\epsilon''$  and  $M''$  (the  
 1407 latter being higher). The geometric factor is probably the largest source of uncertainty in  
 1408 estimating the values of the circuit parameters.

1409 The Maxwell-Wagner equivalent circuit discussed here is obviously crude but serves to  
 1410 rationalize the remarkable success of the electric modulus in analyzing the Maxwell-Wagner  
 1411 effect for water droplets in a dielectric medium of low permittivity.

1412

### 1413 2.3.8.3 Hydration Water

1414 Water of ionic hydration is readily probed by temperature domain dielectric relaxation if  
 1415 the ionic conductivity contribution to  $\epsilon''$  and  $\tan \delta$  is sufficiently small, such as sometimes  
 1416 occurs in hydrate glasses. Data for  $\text{Ca}(\text{NO}_3)_2$  hydrate glasses [39] provide a convenient  
 1417 illustration of how water in different molecular environments can be distinguished dielectrically.  
 1418 Spectra of dielectric  $\tan \delta$  vs.  $1/T$  at 1 Hz were shown for eight glasses of composition  
 1419  $\text{Ca}(\text{NO}_3)_2 \cdot R\text{H}_2\text{O}$  ( $R = 3, 4, 5, 6, 8, 10, 12, 14$ ). Glasses with lower  $R$  values required the  
 1420 addition of  $\text{KNO}_3$  to ensure glass formation but this was expected to have only a minor effect on  
 1421 water dynamics because water was expected to be much more strongly bound to  $\text{Ca}^{2+}$  because of  
 1422 its larger ionic charge/radius compared with  $\text{K}^+$ . Four relaxations were observed labeled as  $\alpha$ ,  $\beta$ ,  $\gamma$ ,  
 1423  $\delta$ :

1424 ( $\alpha$ ) A conductivity relaxation at low  $1/T$  corresponding to the onset of conductivity at glass  
 1425 transition was manifested as a steep increase in  $\tan \delta$ . The relaxation temperature corresponds to  
 1426  $\tan \delta = 1$  and will be referred to here as the "conductivity wing". It is essential that this relaxation  
 1427 occur at sufficiently high  $T$  in order that the other relaxations occur in the poorly conducting  
 1428 glassy state and not be hidden beneath the conductivity contribution to  $\tan \delta$ .

1429 ( $\beta$ ) A dielectric relaxation lying close to the conductivity wing whose shift in position with  $R$   
 1430 paralleled that of the conductivity relaxation. It was observable only as a shoulder for  $R = 1-6$   
 1431 and (probably)  $R = 10$  but is seen as a distinct peak for  $R \approx \text{trace}$ .

1432 ( $\gamma$ ) A weak low temperature dielectric relaxation ( $\tan \delta_{\max} \approx 10^{-3} - 10^{-2}$ ) was observed as a  
 1433 broad maximum for  $R = 4, 5, 6$  and as a shoulder for  $R \geq 8$ .

1434 ( $\delta$ ) A dielectric relaxation whose intensity increased rapidly with  $R$ . It was probably a part of  
 1435 the broad maximum near  $10^3/T \approx 7.5$  for  $R = 8$  but appeared as a clear maximum for  $R \geq 10$ .

1436 The  $\beta$  relaxation was assigned to cation bound water that for the reason given above  
 1437 probably coordinates  $\text{Ca}^+$  rather than  $\text{K}^+$ . The rapid shift in relaxation temperature with  $R > 1$  was  
 1438 interpreted as a change in water dynamics as  $\text{H}_2\text{O}$  replaces  $\text{NO}_3^-$  in the first coordination shell of  
 1439  $\text{Ca}^+$ . The  $R$  invariance for  $R = \text{trace}$  and  $R = 1$  was attributed to a single water molecule lying in  
 1440 the first coordination shell. This assignment of the  $\beta$  relaxation to  $\text{Ca}^{2+}$  bound water implied a  
 1441 dielectric activity that merits discussion. The most plausible geometry for  $\text{H}_2\text{O}$  coordinated to  $\text{Ca}^+$   
 1442 is when the  $\text{H}_2\text{O}$  dipole points away from the  $\text{Ca}^+$  ion. However if this held in the complex ionic  
 1443 environment of the glass there would be no dielectric activity because the rotational axis would  
 1444 bisect the H-O-H angle and coincide with the dipole vector. Two alternatives suggest themselves:  
 1445 (1) Exchange of water and nitrate in the coordination shell. This implies an associated volume  
 1446 fluctuation and ultrasonic activity. Such activity has been observed [40,41] in  $\text{Ca}(\text{NO}_3)_2 \cdot R\text{H}_2\text{O}$   
 1447 solutions at about 20 MHz at room temperature. This relaxation moved to higher frequencies with  
 1448 increasing  $R$  and the edge of a second relaxation at higher frequencies was noted, both being  
 1449 consistent with the glassy state dielectric behavior. Such an exchange would also be expected to  
 1450 contribute to the translational ionic migration that produces conductivity, consistent with the  
 1451 essentially  $R$  – invariant difference between the  $\alpha$  and  $\beta$  relaxation temperatures. The  
 1452 possibility that this relaxation is part of a conductivity relaxation with a distribution of relaxation  
 1453 times is discussed in §2.5.

1454 (2) A different  $\text{Ca}^+ \text{-OH}_2$  geometry in which the dipole vector and rotation axis do not  
 1455 coincide. Neutron diffraction data indicate this occurs in  $\text{CaCl}_2$  and  $\text{NiCl}_2$  solutions [42], in  
 1456 which an angle of ca.  $40^\circ$  was observed between the dipole and coordination axes at  $R = 12.6$   
 1457 ( $\text{NiCl}_2$ ) and 12.3 ( $\text{CaCl}_2$ ), and about  $0^\circ$  in dilute solutions ( $R \approx 450$ ). It was not possible to find  
 1458 the dielectric activity per water molecule of the  $\beta$  relaxation in the  $\text{Ca}(\text{NO}_3)_2 \cdot R\text{H}_2\text{O}$  glasses  
 1459 because of overlap with the conductivity wing and the  $\gamma$  relaxation, but for the mixed nitrate  
 1460 glasses the well defined conductivity wing for the anhydrous mixture could be shifted and  
 1461 subtracted to yield plausibly shaped peaks of  $\tan \delta$  vs.  $1/T$ . The peak heights and widths in the  $R$   
 1462 = 1 and  $R = 3$  glasses were about the same so that barring an unlikely ratio of activation energies  
 1463 in excess of 3 it appears that the dielectric activity per water molecule does indeed decrease with  
 1464 increasing  $R$ . A crude calculation yielded sensible values of  $\Delta\theta$  from the observed values of  
 1465  $\tan \delta_{\text{max}}$ : the dipole being relaxed was assumed to be the component of the water dipole ( $\mu_w$ )  
 1466 orthogonal to the rotation axis, magnitude  $\mu_w \sin(\Delta\theta)$ , and  $\tan \delta_{\text{max}}$  was assumed to be  
 1467 proportional to  $(\epsilon_0 - \epsilon_\infty)$  that is in turn proportional to  $R[\mu_w \sin(\Delta\theta)]^2$ . Equating  $\tan \delta_{\text{max}}$  for  
 1468 the  $1R$  and  $3R$  glasses then yielded

$$1470 \quad \frac{3}{T_{3R}} \sin^2(\Delta\theta_{3R}) = \frac{1}{T_{1R}} \sin^2(\Delta\theta_{1R}), \quad (2.183)$$

1471  
 1472 so that  
 1473

$$\sin^2(\Delta\theta_{3R}) \approx 0.286 \sin^2(\Delta\theta_{1R}). \quad (2.184)$$

1475  
1476 Examples of  $\{\Delta\theta_{1R}, \Delta\theta_{3R}\}$  pairs were  $\{60^\circ, 28^\circ\}$  and  $\{30^\circ, 15^\circ\}$ , both sensible values and roughly  
1477 comparable with the neutron diffraction values.

1478 For large values of  $R$  the  $\delta$  relaxation was expected to resemble that of pure water so that  
1479 an extrapolation to infinite dilution could yield the temperature at which the relaxation frequency  
1480 of water is 1 Hz. The relaxation temperatures at 1 Hz for the  $\delta$  relaxation in four glasses  
1481 ( $\text{Ca}(\text{NO}_3)_2$ ,  $\text{CaZnCl}_4$ ,  $\text{Li}_2\text{ZnCl}_4$  and  $\text{ZnCl}_2$  hydrates) all extrapolated to  $162 \pm 5$  K at infinite  
1482 dilution, suggesting that the relaxation temperature for pure water would be  $162 \pm 5$  K at 1Hz.  
1483 The temperature dependence of the relaxation time for water between  $-20^\circ\text{C}$  to  $+30^\circ\text{C}$  [43] was  
1484 found to follow the Fulcher equation

$$\tau(T) = A_F \exp\left(\frac{B_F}{T - T_0}\right) \quad (2.185)$$

1487  
1488 with  $A_F = 1.25 \times 10^{-13}$  s,  $B_F = 669$  K,  $T_0 = 138$  K. The extrapolated  $\{1 \text{ Hz}, 162 \pm 5 \text{ K}\}$  datum  
1489 agreed with the predicted Fulcher value  $\{1 \text{ Hz}, 162 \text{ K}\}$ . Given the large extrapolation over about  
1490 11 orders of magnitude (!) this agreement constitutes good evidence that dielectric relaxation of  
1491 water outside the first coordination shell of the  $\text{Ca}^{2+}$  and  $\text{Li}^+$  cations is the same as pure water.  
1492 This was supported by a similar extrapolation of LiCl in glycerol data that yielded a relaxation  
1493 temperature equal to the directly observable value for pure glycerol at 1 Hz.

## 1494 2.4 Conductivity Relaxation

### 1495 2.4.1 General Aspects

1497 As noted earlier, relaxation of polarization can occur either by translation of electric  
1498 charge (electric current) or by dipole rotation/localized ion hopping (displacement current). Thus  
1499 polarization induced by an electric field can occur by conductivity relaxation [44] arising from  
1500 long range translational migration of point charges as well as by the dielectric relaxation  
1501 considered so far. The time scale associated with a frequency invariant conductivity  $\sigma_0$  is defined  
1502 by (eq. 1.42)

$$\langle \tau_D \rangle = \sigma_0 / e_0 \epsilon_\infty, \quad (2.186)$$

1505  
1506 but this is not evident in  $\sigma'$  vs  $\ln \omega$  plots nor is it for the function  $\epsilon^* = \epsilon' - i\sigma_0 / e_0 \omega$ . However  
1507  $\rho''$  and  $M''$  clearly indicate the time scale because they exhibit maxima in the frequency domain  
1508 at  $\omega \approx 1 / \langle \tau_D \rangle$ . The time constant  $\tau_D$  in eq. (2.186) differs from the characteristic time  $\tau_e$  in the  
1509 Fermi gas expression for electronic conductivity in metals that is directly proportional to  $\sigma_0$  [45]:

$$\tau_e = \frac{m}{ne^2} \sigma_0, \quad (2.187)$$

1512  
 1513 where  $n$  is the number density of charge carriers of effective mass  $m$  and charge  $e$ . The reason for  
 1514 the difference is that  $\tau_e$  is the average time of travel between scattering events (collisions with  
 1515 ions, electrons, phonons or by umklapp), whereas  $\tau_D$  is the residence time between (effectively  
 1516 instantaneous) jumps between adjacent sites. Nor is  $\tau_D$  equal to  $\tau_E$  for dielectric relaxation,  
 1517 although they are related by an expression that is derived below.

1518 Equation (2.186) implies that ionic conductivity cannot exceed ca.  $10^3 \text{ Sm}^{-1}$ , since  $\tau_D$   
 1519 cannot reasonably be less than a vibrational lifetime  $\tau_v$  and  $\epsilon_\infty$  is rarely greater than about 10.  
 1520 The vibrational lifetime is conveniently defined by the condition for critical damping (§1.11),  
 1521  $\omega_0 \tau_v = 1$ , so that for a typical vibrational frequency of about  $f \approx 10^{12} \text{ Hz} \Rightarrow \omega \approx 6 \times 10^{12} \text{ rad/s}$  the  
 1522 value of  $\tau_v$  is about  $2 \times 10^{-13} \text{ s}$  and

$$1523 \quad \sigma_{0,\text{max}} \approx \frac{e_0 \epsilon_\infty}{\tau_v} \approx \frac{(8.854 \times 10^{-12} \text{ F/m})(10)}{2 \times 10^{-13} \text{ s}} \approx 450 \text{ S/m}, \quad (2.188)$$

1525  
 1526 comparable with the highest conductivity observed for ionic conductors.

1527 The properties of the four basic functions for conductivity relaxation (eq. (2.106)) are  
 1528 conveniently illustrated using a circuit comprising three elements in series: (i) a capacitance  
 1529  $C_s = 10^{-6} \text{ F} = 1 \mu\text{F}$ ; (ii) a parallel combination of a resistance  $R_1 = 10^8 \Omega$  and capacitance  
 1530  $C_1 = 10^{-12} \text{ F} (1 \text{ pF})$  (iii) another parallel combination of a resistance  $R_2 = 10^6 \Omega$  and capacitance  
 1531  $C_1 = 10^{-12} \text{ F} (1 \text{ pF})$ . The two parallel  $R_p$ - $C_p$  elements could for example simulate crystal and inter-  
 1532 crystal impedances in a polycrystalline samples and the series capacitance  $C_s$  could simulate  
 1533 electrode polarization. As discussed below this circuit has been used by several groups and will  
 1534 be referred to as the "ideal" conductivity circuit.

1535 The electric modulus  $M^* = M' + iM''$  is particularly useful for analyzing conductivity  
 1536 relaxation but it is controversial (a discussion of many of the issues is given in [1]). It was  
 1537 probably first defined by McCrum, Read and Williams [32], but its use in analyzing conductivity  
 1538 relaxation was initiated by Macedo and coworkers [44]. The usefulness of  $M^*$  is illustrated by the  
 1539 simplest case of a constant conductivity  $\sigma_0$  and constant relative permittivity  $\epsilon_\infty$  (the reason for  
 1540 the subscripts will become clear when distribution functions are considered later). Consider the  
 1541 definitions

$$1542 \quad M' = \frac{\epsilon'}{\epsilon'^2 + \epsilon''^2} \quad (a),$$

$$1543 \quad M'' = \frac{\epsilon''}{\epsilon'^2 + \epsilon''^2} \quad (b). \quad (2.189)$$

1544  
 1545 Insertion of the relations  $\epsilon'' = \sigma_0 / e_0 \omega$  and  $\epsilon' = \epsilon_\infty$  then yields

1546

$$1547 \quad M' = \frac{1}{\varepsilon_{\infty}^D} \left( \frac{\omega^2 \tau_D^2}{1 + \omega^2 \tau_D^2} \right) \quad (2.190)$$

1548  
1549 and  
1550

$$1551 \quad M'' = \frac{1}{\varepsilon_{\infty}^D} \left( \frac{\omega \tau_D}{1 + \omega^2 \tau_D^2} \right). \quad (2.191)$$

1552  
1553 Thus  $M''$  exhibits a desirable peak centered at  $\omega_D = 1/\tau_D$  as a function of  $\ln(\omega)$ . The components  
1554 of the complex resistivity  $\rho^*$  are related to those of  $M^*$  by (eq. (2.106))  
1555

$$1556 \quad \rho' = \frac{M''}{e_0 \omega} = \frac{\tau_D}{e_0 \varepsilon_{\infty}^D} \left( \frac{1}{1 + \omega^2 \tau_D^2} \right) = \left( \frac{\rho_0}{1 + \omega^2 \tau_D^2} \right) \quad (2.192)$$

1557  
1558 and  
1559

$$1560 \quad \rho'' = \frac{M'}{e_0 \omega} = \frac{\tau_D}{e_0 \varepsilon_{\infty}^D} \left( \frac{\omega \tau_D}{1 + \omega^2 \tau_D^2} \right) = \rho_0 \left( \frac{\omega \tau_D}{1 + \omega^2 \tau_D^2} \right), \quad (2.193)$$

1561  
1562 where  $\rho_0 = 1/\sigma_0 = \tau_D / e_0 \varepsilon_{\infty}^D$ . The functions  $M''$  and  $\rho''$  have identical frequency dependencies  
1563 but are weighted by  $1/\varepsilon_{\infty}$  and  $\rho_0$  respectively. The difference in weighting factors can be exploited  
1564 to considerable advantage in the analysis of ac conductivity data (§2.3.5.6 - §2.3.5.8).

1565 For dielectric relaxation  $M^*$  and  $\varepsilon^*$  are almost equivalent because a Debye peak in  $\varepsilon''$   
1566 also yields a Debye peak in  $M''$  [44] [see eqs. (2.132) and (2.133)]. The derivation of  $M^*$  for a  
1567 Debye dielectric without any conductivity is given in Appendix 2.1. It might appear that a peak in  
1568  $M''$  could be due to either a conductivity or dielectric process and that  $M^*$  could not distinguish  
1569 between them but this is not necessarily so because the average relaxation time  $\langle \tau_D \rangle$  will be  
1570 calculable from the limiting low frequency conductivity [eq. (2.73)] if the process is a  
1571 conductivity relaxation, and the retardation time will not correlate with  $\sigma_0$  if the peak in  $M''$  is  
1572 due to a dielectric relaxation Also  $\lim_{\omega \rightarrow 0} M'(\omega) = 1/\varepsilon_0$  for dielectric relaxation compared with  
1573  $\lim_{\omega \rightarrow 0} M'_{conductivity}(\omega) = 0$  for conductivity relaxation. The archetypal example of dielectric  
1574 relaxation being correlated with  $\sigma_0$  occurs in the alkali silicate glasses and it was this correlation  
1575 that originally led to the inference that the residual dielectric loss (after subtraction of  $\sigma_0 / e_0 \omega$ ) is  
1576 due to the same alkali migration process that produces  $\sigma_0$  [27-31]. This led Macedo and  
1577 collaborators [44] to first use  $M^*$  in the analysis of conductivity relaxation.

1578 The low frequency conductivity relaxation limit for  $M'$  is revealing because  $M'$  is a  
1579 measure of the restoring force in response to an electric field perturbation. The low frequency  
1580 limit of this restoring force is finite for dielectric relaxation because the charge storage ability

1581 remains nonzero:  $\lim_{\omega \rightarrow \infty} \varepsilon'(\omega) = \varepsilon_0$ . For conductivity relaxation the dielectric loss becomes infinite  
 1582 as  $\omega \rightarrow 0$  (dissipation completely overrides any storage capability) and the restoring force is  
 1583 “short circuited”. This is precisely analogous to the mechanical modulus going to zero as the  
 1584 viscosity of a viscoelastic material dominates at low frequency and the elasticity disappears. The  
 1585 electric modulus was first introduced to emphasize this mechanical analogy [32].

1586 An alternative to the electric modulus for analyzing materials in which the dielectric loss  
 1587 and conductivity are correlated has been proposed by Johari [46]. This proposal is similar in style  
 1588 to a mechanism for ionic conductivity proposed by Hodge and Angell [47] that was based on the  
 1589 one-dimensional Glarum diffusion model for dielectric relaxation [§1.12.6, Chapter One]. The  
 1590 Glarum model comprises a relaxing dipole that can relax either independently with retardation  
 1591 time  $\tau_0$  or by the arrival of a defect of some kind that relaxes it instantly. Hodge and Angell  
 1592 suggested that the dipole is a trapped ion/vacancy pair (known to exhibit Debye dielectric  
 1593 behavior, §2.3.1.2) and that the defects are itinerant ions that contribute to  $\sigma_0$ . Such diffusing  
 1594 ions would eliminate the dipole upon arriving by inserting themselves into the vacancy, consistent  
 1595 with the Glarum model. The average activation energy for oscillation of trapped ions and that for  
 1596 ion migration are presumed to be similar (perhaps identical), thus accounting for the nearly  
 1597 temperature invariant distribution of conductivity relaxation times. The Glarum function is  
 1598 mathematically similar to the Davidson-Cole function that has a (rarely observed) Debye-like low  
 1599 frequency loss. This low frequency behavior arises from the Glarum assumption that the dipole  
 1600 has just one retardation time. However if a distribution of dipole retardation times is assumed,  
 1601 corresponding to a distribution of sites in an amorphous material and/or local fields effects  
 1602 (§2.3.1.2) for example, better agreement with experiment might be obtained without changing the  
 1603 essential physics of the Glarum model.

1604

#### 1605 2.4.2 Distribution of Conductivity Relaxation Times

1606 Both  $M^*$  and  $\rho^*$  can be formally described in terms of a distribution of conductivity  
 1607 relaxation times:

1608

$$1609 \quad M^*(i\omega) = M_\infty \int_{-\infty}^{+\infty} g(\ln \tau_D) \left( \frac{i\omega\tau_D}{1 + \omega^2\tau_D^2} \right) d \ln \tau_D \quad (2.194)$$

1610

1611 and similarly for  $\rho^*(i\omega)$ . A distribution of conductivity relaxation times affects the dispersion  
 1612 of the corresponding complex admittance functions  $\varepsilon^*(i\omega)$  and  $\sigma^*(i\omega)$ :

1613

$$1614 \quad \sigma_0 = \frac{e_0 \varepsilon_\infty^D}{\langle \tau_D \rangle} = \frac{e_0}{M_\infty^D \langle \tau_D \rangle}, \quad (2.195)$$

$$1615 \quad \sigma_\infty = e_0 \varepsilon_\infty^D \left\langle \frac{1}{\tau_D} \right\rangle = \frac{e_0}{M_\infty^D} \left\langle \frac{1}{\tau_D} \right\rangle, \quad (2.196)$$

1616

1617 and

1618

$$\varepsilon_0^D = \varepsilon_\infty^D \frac{\langle \tau_D^2 \rangle}{\langle \tau_D \rangle^2} \geq \varepsilon_\infty^D, \quad (2.197)$$

1620

1621 where the subscripts 0 and  $\infty$  denote limiting low and high frequency limits respectively. Also, the  
 1622 commonly observed limiting high frequency power law behavior  $\sigma'(\omega) \propto \omega^n$  ( $0 \leq n \leq 1$ ) depends  
 1623 on the distribution: the broader the distribution the closer  $n$  is to unity. Values of  $n$  greater than  
 1624 unity imply that a resonance process occurs at higher frequencies (see below §2.4.3).

1625 A distribution of conductivity relaxation times is not easily distinguishable from dielectric  
 1626 and conductivity relaxations occurring together [36,44], although the dielectric relaxation will not  
 1627 be observable if  $\tau_E \gg \tau_D$  because  $\sigma_0$  will then exceed the limiting high frequency dielectric  
 1628 conductivity given by eq. (2.131):

1629

$$\frac{\sigma'(\omega\tau_D \rightarrow 0)}{\sigma_\mu(\omega\tau_E \rightarrow \infty)} = \frac{\sigma_0}{\sigma_\mu(\infty)} = \frac{\varepsilon_\infty}{\langle \tau_D \rangle} \left( \frac{\langle \tau_E \rangle}{\varepsilon_0 - \varepsilon_\infty} \right) = \frac{\varepsilon_\infty}{\varepsilon_0 - \varepsilon_\infty} \frac{\langle \tau_E \rangle}{\langle \tau_D \rangle} \gg 1. \quad (2.198)$$

1631

1632 This phenomenon has been directly observed in systems for which the dielectric retardation time  
 1633 is essentially constant but whose conductivity is increased by addition of electrolyte [48, 49] (also  
 1634 see §2.3.6.9 below).

1635

### 1636 2.4.3 Contribution of Resonance Absorption

1637 If a resonance process occurs that is centered at a much higher frequency than  
 1638  $\omega_D = e_0 \varepsilon_\infty / \sigma_0$  (eq. (2.186)) then the conductivity can increase more rapidly with frequency than  
 1639 the maximum proportionality to  $\omega$  for a relaxation process. This is clear from the low frequency  
 1640 limit of eq. 1.395 in Chapter 1 for the resonance expression for the dielectric loss:

1641

$$\varepsilon''(\omega) = \propto \omega \quad (2.199)$$

1643

1644 that implies a low frequency limit  $\sigma_{resonance} \propto \omega^2$ . This can yield a power law relation  $\sigma \propto \omega^a$  for  
 1645 which  $a > 1$ .

1646

### 1647 2.4.4 Constant Phase Element Analysis

1648 It is sometimes useful to have a circuit element for which the phase angle is independent  
 1649 of  $\omega$ ,

1650

$$W^*(i\omega) = W(\omega) \exp\left(\frac{\pm i \alpha \pi}{2}\right), \quad (2.200)$$

1652

1653 where  $W(\omega)$  is any real function and  $0 < \alpha \leq 1$  is also real (the positive sign in the exponent  
 1654 corresponds to an admittance and the negative sign to an impedance). However as noted in  
 1655 Chapter One and §2.4.3 eq. (2.200) can only be valid over a restricted frequency range because

1656 otherwise the underlying distribution of relaxation/retardation times cannot be normalized.  
 1657 Equation (2.200) is a generalization of the Warburg impedance for which  $\alpha = 0.5$ .

1658

#### 1659 2.4.5 Estimation of $\sigma_0$

1660 Several methods have been published for estimating  $\sigma_0$  in situations where it has been  
 1661 contaminated by such factors as electrode polarization and intergranular impedances. An accurate  
 1662 value for  $\sigma_0$  is often important because, in addition to the obvious need for reliable data, its  
 1663 contribution to  $\varepsilon''$  must be subtracted for permittivity analyses (the attendant difficulties have  
 1664 been discussed by Ravaine and Souquet [52, 53]). Accurate values of  $\sigma_0$  are also needed in order  
 1665 to determine reliable activation energies for conductivity. For example if  $\log(\sigma)$  measured at

1666 constant measuring frequency  $\omega_{meas}$  is plotted against  $1/T$  in the usual Arrhenius fashion then  
 1667 spurious changes in slope can result from both electrode polarization and bulk relaxation effects.

1668 (1) If the measuring frequency  $\omega_{meas}$  is so low that polarization is significant then the  
 1669 measured conductivity will be less than  $\sigma_0$ , by an amount that increases with increasing  
 1670 temperature because of the shift to higher frequencies of the polarization  $\sigma'$  spectrum (which has  
 1671 essentially the same effective activation energy as the sample conductivity).

1672 (2) A fictitiously low activation energy is then obtained at high temperatures as  $\omega_{meas}$  probes  
 1673 deeper into the polarization relaxation. A spuriously low activation energy can also occur at low  
 1674 temperatures when  $\omega_{meas}$  lies within the bulk relaxation frequency range where  $\sigma'$  is often  
 1675 observed to increase as  $\omega^\alpha$  ( $\alpha < 1$ ). In this case the measured conductivity will exceed  $\sigma_0$  by an  
 1676 amount that decreases with increasing temperature and the measured activation energy will be  
 1677 smaller than the true value by the factor  $\alpha = d \ln \sigma' / d \ln \omega$ :

1678

$$1679 \quad E_{a,obs} = E_{a,true} (1 - \alpha). \quad (2.201)$$

1680

1681 In cases where  $\alpha \approx 1$ , as occurs in some electronic semiconductors [48], the fixed frequency  
 1682 conductivity is therefore almost independent of temperature in the bulk relaxation temperature  
 1683 region.

1684

#### 1685 2.4.5.1 Analyses in the Complex Resistivity Plane

1686 Ravaine and Souquet [52,53] used the complex resistivity plane for determining  $\sigma_0$  of  
 1687 alkali silicate glasses in the presence of electrode polarization using low frequency extrapolations  
 1688 to the real axis. They fitted the high frequency spectrum (i.e. sample relaxation) to the Cole-Cole  
 1689 [54] function (§1.12.5) and extrapolated the Cole-Cole semicircle to the real axis. For severe  
 1690 polarization Armstrong et al. [55-59] used a similar method based on extrapolation of the high  
 1691 frequency polarization spike to the real axis. This method is restricted to high conductivities  
 1692 whose relaxation frequency lies above the measuring frequency range.

1693

#### 1694 2.4.5.2 Modulus and Resistivity Spectra

1695 In cases where electrode polarization and conductivity relaxations overlap significantly

1696 and no plateau in  $\sigma'$  is observed,  $\sigma_0$  can be estimated from eq. (2.186) if  $\langle\tau_D\rangle$  and  $\varepsilon_\infty$  are known.  
 1697 These can sometimes be determined with sufficient precision by fitting  $M''(\omega)$  to an appropriate  
 1698 empirical function because  $M''$  is insensitive to high capacitance effects such as electrode  
 1699 polarization and intergranular impedances so that only the bulk relaxation is included in the fitted  
 1700 function. For this application the fit to  $M''$  should preferably be weighted by the lower frequency  
 1701 data because these reflect the longer relaxation time components of the distribution that contribute  
 1702 more significantly to  $\langle\tau_D\rangle$ . The maximum in  $\rho''$ ,  $\rho''_{\max}$ , can also be used to estimate  $\sigma_0$  to within  
 1703 about 10% if the full width at half height of the peak in  $\rho''$  ( $\Delta$  decades) can be determined:

$$1705 \quad \sigma_0 \approx \frac{1}{1.75 \Delta \rho''_{\max}}. \quad (2.202)$$

1706  
 1707 If only the maximum in  $\rho''$  at  $\omega_{\max}$  is observable  $\sigma_0$  can still be estimated from the value of  $\rho'$   
 1708 at  $\omega_{\max}$  by assuming  $\rho''(\ln \omega)$  to be symmetric:

$$1710 \quad \sigma_0 \approx \frac{1}{2\rho'(\omega_{\max})}. \quad (2.203)$$

### 1711 2.4.5.3 Complex Admittance Plane

1712 One of the first applications of complex plane plots was to polycrystalline yttria-zirconia  
 1713 electrolytes by Bauerle [60]. Bauerle gave an excellent discussion of equivalent circuits and their  
 1714 corresponding complex admittance plane plots, but the only circuit used in their data analysis was  
 1715 a series combination of two parallel  $R_pC_p$  elements and a series resistance  $R_s$ . The first parallel  
 1716  $R_pC_p$  element in this circuit represented the electrode interface: the capacitance of a double layer  
 1717 in parallel with the resistance of an oxygen gas-oxide ion charge transfer process. The second  
 1718  $R_pC_p$  element represented an intergranular boundary ("constriction") impedance, and the pure  
 1719 resistance simulated the bulk crystal. The experimentally observed complex admittance plane  
 1720 plots were in excellent agreement with the equivalent circuit predictions. The zero frequency  
 1721 conductivity predicted from the complex plane plot was also in excellent agreement with four  
 1722 terminal data, and the expected dependence of the electrode impedance on oxygen partial pressure  
 1723 was observed. Despite these successes, some disadvantages of the method should be pointed out.  
 1724 First, in assuming that the bulk crystal acts as a pure resistance the analysis implicitly assumes  
 1725 that the measuring frequencies are well below the conductivity relaxation frequency, that can only  
 1726 be confirmed retrospectively. Second, although there are three relaxing elements (since the  
 1727 sample resistance must realistically have a capacitance in parallel with it), the complex admittance  
 1728 plane exhibits only two arcs that reflect the differences between the relaxing elements. If the  
 1729 observed relaxations overlap significantly, an assumption must be made about the shapes of the  
 1730 two relaxations before extrapolations are made, i.e. a functional form for the extrapolating  
 1731 function must be chosen. Bauerle's data were well described by the Cole-Cole function but this  
 1732 would not be expected to occur in general.

1734

## 1735 2.4.6 Examples

## 1736 2.4.6.1 Electrode Polarization and Bulk Relaxation in the Frequency Domain

1737 Consider an "ideal" equivalent circuit similar to that used by Bauerle except that the series  
 1738 resistance is replaced by a series capacitance, with specific values of the parallel  $R_p C_p$  elements  
 1739 being  $[R_1 = 10^8 \Omega, C_1 = 10^{-11} \text{F} \Rightarrow \tau_1 = R_1 C_1 = 10^{-3} \text{s}]$ ,  $[R_2 = 10^6 \Omega, C_2 = 10^{-11} \text{F} \Rightarrow \tau_2 = R_2 C_2 = 10^{-5} \text{s}]$   
 1740 and  $[C_s = 10^{-6} \text{F}]$ . The distribution of conductivity relaxation times then comprises two delta  
 1741 functions at  $\tau_1 = 10^{-3} \text{s}$  and  $\tau_2 = 10^{-5} \text{s}$ . The shorter relaxation time element simulates the crystal  
 1742 impedance in a polycrystalline preparation, the longer relaxation time element simulates an  
 1743 intergranular impedance, and the series capacitance simulates electrode polarization. This circuit  
 1744 has been found to be useful in analyzing the electric response of a variety of conducting materials,  
 1745 including a superionic conductor [61], an electronic semiconductor [62], and a normal ionic  
 1746 conductor [9]. The relaxation time averages are

$$1748 \quad \langle \tau_D^2 \rangle = \frac{\tau_1^2 + \tau_2^2}{2} = 5.0005 \times 10^{-9} \text{ s} \quad (2.204)$$

$$1749 \quad \langle \tau_D \rangle = \frac{\tau_1 + \tau_2}{2} = 5.05 \times 10^{-5} \text{ s} \quad (2.205)$$

$$1750 \quad \langle \tau_D^{-1} \rangle = \frac{\tau_1^{-1} + \tau_2^{-1}}{2} = 5.05 \times 10^{+5} \text{ s} \quad (2.206)$$

1751  
 1752 The high frequency relative permittivity is (assuming  $k = 1$  for convenience so that  $C_0 = \epsilon_0$   
 1753 numerically)

$$1755 \quad \epsilon_\infty = \frac{C_1 C_2}{\epsilon_0 (C_1 + C_2)} = 5.647, \quad (2.207)$$

1756  
 1757 and the low frequency relative permittivity is

$$1759 \quad \epsilon_0 = \epsilon_\infty \frac{\langle \tau_D^2 \rangle}{\langle \tau_D \rangle^2} = (5.647) \frac{(5.005 \times 10^{-9})}{(5.05 \times 10^{-5})^2} = 11.083. \quad (2.208)$$

1760  
 1761 The limiting low and high frequency conductivities are

$$1763 \quad \sigma_0 = \frac{\epsilon_0 \epsilon_\infty}{\langle \tau_D \rangle} = \frac{(8.854 \times 10^{-12})(5.647)}{(5.05 \times 10^{-5})} = 9.9 \times 10^{-7} \text{ S m}^{-1} \quad (2.209)$$

$$1764 \quad \sigma_\infty = \epsilon_0 \epsilon_\infty \langle 1/\tau_D \rangle = (8.854 \times 10^{-12})(5.647)(5.05 \times 10^{+5}) = 2.53 \times 10^{-5} \text{ Sm}^{-1}. \quad (2.210)$$

1765  
 1766 (1) The  $\rho''$  and  $M''$  spectra both exhibit two peaks the heights of which reflect the different

1767 weighting of the two functions - eqs. (2.191) and (2.193). The two  $\rho''$  peak heights differ by the  
 1768 ratio of the resistances  $10^8/10^6 = 10^2$ , whereas the  $M''$  peaks are equal in height because the two  
 1769 capacitances are equal. If the capacitances were different and the resistances the same then the  
 1770 peaks in  $\rho''$  would have the same height and those in  $M''$  would differ. Also  $\rho''$  increases  
 1771 indefinitely at low frequencies due to  $C_s$  whereas  $M''$  is unaffected.

1772 (2) After subtraction of the contribution of  $\sigma_0$  to  $\epsilon''$ , and of the limiting high frequency  
 1773 contribution of  $\epsilon_\infty$  to  $\sigma''$ , both  $\sigma''$  and  $\epsilon''$  exhibit a single peak at a frequency between the two  
 1774 maxima exhibited in the  $M''$  and  $\rho''$  spectra. These single peaks in the admittance functions occur  
 1775 because at intermediate frequencies the high frequency  $RC$  element behaves as a resistance and  
 1776 the low frequency  $RC$  element behaves as a capacitance. As noted in §2.2.4 the effectively series  
 1777  $RC$  circuit will produce just a single loss peak in the admittance. For the electrode polarization  
 1778 relaxation caused by  $C_s$  in series with the sample resistance  $(R_1 + R_2)$  peaks in  $\sigma'' - e_0 \epsilon_\infty \omega$  and  
 1779  $\epsilon'' - \sigma_0 / e_0 \omega$  are observed at lower frequencies.

1780 (3) A low frequency decrease in  $\sigma'$  and increases in  $\epsilon'$  and  $\rho''$  are found that are due to the  
 1781 electrode polarization simulated by  $C_s$ . For expositional clarity the value of  $C_s$  was chosen to  
 1782 ensure a clean separation between the simulated polarization and bulk relaxations but this does  
 1783 not occur in typical experimental data.

1784 (4) The complex plane plots have both advantages and disadvantages compared with the  
 1785 spectra. Two disadvantages are the inconvenience of locating the frequencies of maximum loss,  
 1786 and of comparing these frequencies in  $M^*$  and  $\rho^*$  plots because of the opposite directions of  
 1787 increasing frequency. On the other hand, complex plane plots are useful for extrapolations. For  
 1788 example in highly conducting materials whose conductivity relaxation frequency  $1/\langle\tau_D\rangle$  lies  
 1789 above the measuring frequency, and for which electrode polarization is significant or even severe,  
 1790 the polarization spike in the  $\rho^*$  plane can be extrapolated to the real axis to give an estimate of  
 1791  $\sigma_0 = 1/\rho_0$ . At frequencies above the conductivity relaxation frequency,  $\sigma_0$  is manifested as a  
 1792 spike in the  $\epsilon^*$  plane, corresponding to the limiting values of  $\lim_{\omega \rightarrow 0} \epsilon'' = \lim_{\omega \rightarrow 0} \sigma_0 / e_0 \omega = \infty$  and  
 1793  $\lim_{\omega \rightarrow 0} \epsilon' = \epsilon_0$ .

#### 1794 2.4.6.2 Conductivity Relaxation in Sodium $\beta$ -Alumina

1796 Permittivity, modulus and resistivity spectra of single crystal sodium  $\beta$ -alumina at 113 K  
 1797 have been reported by Grant and Ingram [64,65]:

- 1798 (i) the  $\epsilon''$  spectrum measured in the direction perpendicular to the conduction planes;
- 1799 (ii) the  $M''$  spectra in orientations perpendicular and parallel to the conducting planes;
- 1800 (iii) the  $Z''$  spectrum measured in the direction of the conduction planes.

1801 The frequency of maximum  $Z''$  in the parallel orientation was close to the frequency of  
 1802 maxima in  $M''$  and  $\epsilon''$  measured in the perpendicular orientation, and the activation energy for the  
 1803 parallel resistivity spectrum was close to that for the perpendicular dielectric loss spectrum. The  
 1804 data for the perpendicular orientation were interpreted in terms of a Maxwell layered dielectric  
 1805 [65], with each insulating spinel block being a capacitance and each conduction plane a  
 1806 resistance. The activation energy for the dielectric loss was thus determined by that of the

1807 conductivity of the conducting layers, that the data suggest is similar in directions parallel and  
1808 perpendicular to the conduction planes. An extraordinarily large width of the  $M''$  spectrum for  
1809 single crystal Na  $\beta$ -alumina was observed in the parallel orientation [66,67], indicating a very  
1810 broad distribution of conductivity relaxation times: the resistivity and modulus spectra taken  
1811 together suggested that the distribution was bimodal. Grant and Ingram proposed that at 113 K the  
1812 low frequency conductivity is determined by an activated localized ion motion that is the same in  
1813 both orientations. The higher frequency conductivity, which contributed to  $M''$  but not to  $\rho''$ ,  
1814 resulted from a relatively free motion of ions crossing low energy barriers. These processes were  
1815 consistent with low temperature localization of sodium ions deduced from NMR data [68].  
1816 Localized activation is not the rate determining step at high temperatures and the well-established  
1817 low activation energy for conductivity in sodium  $\beta$ -alumina was observed. Spectra of  $M''$  and  $Z''$   
1818 for a representative polycrystalline specimen at 113 K were also reported. The  $Z''$  spectrum was  
1819 uninformative at this temperature, increasing monotonically at low frequencies due to electrode  
1820 polarization. The  $M''$  spectrum exhibited a maximum at about the same frequency as the single  
1821 crystal  $M''$  spectrum observed perpendicular to the conduction planes, and a reproducible shoulder  
1822 was observed at about the same frequency as  $M''$  observed parallel to the conduction planes in  
1823 single crystals.

1824 This work demonstrates that comparison of the functions  $M''$ ,  $\rho''$  and  $\varepsilon''$  can uncover  
1825 details of the conductivity behavior of sodium  $\beta$ -alumina that could not even be discussed if  
1826 only  $\sigma^*$  and  $\varepsilon^*$  data were used.

#### 1827 1828 2.4.6.3 Complex Impedance Plane Analysis of Electrode Polarization in Sintered $\beta$ - 1829 Alumina.

1830 The use of the complex impedance plane for extrapolating polarization phenomena to  
1831 obtain data on the bulk material was used extensively by Armstrong and coworkers in their  
1832 studies of superionic conductors such as Na  $\beta$ -alumina [55] and Ag-Rb iodide [54-58]. A spike  
1833 in the complex impedance plane corresponds to the low frequency increase in  $Z''$  due to the series  
1834 electrode capacitance and extrapolation of this spike to the real axis yielded the limiting low  
1835 frequency values of  $Z'$  and therefore of  $\rho_0$ . Different surface preparations were observed to  
1836 affect the measured impedance but all of the extrapolations gave the same values for  $\rho_0$ . This  
1837 method is clearly most appropriate for very highly conducting materials whose conductivity  
1838 relaxation lies at frequencies well above those used experimentally.

#### 1839 1840 2.4.6.4 Complex Impedance Plane Analysis of Atmosphere Dependent Electrode Effects in $\text{KHF}_2$

1841 Complex impedance plane analysis was also used by Bruinink and Broers [69] for the  $\alpha$   
1842 and  $\beta$  phases of  $\text{KHF}_2$ . In an atmosphere of hydrogen with platinum paint electrodes, the complex  
1843 impedance plane plot of data for  $\alpha$ - $\text{KHF}_2$  was consistent with a Warburg impedance in parallel  
1844 with the bulk resistance and capacitance [69], and extrapolation to the real axis gave a value of  
1845  $\rho_0$  in agreement with a separately determined four terminal dc value. This plot gave no indication  
1846 of interfacial polarization, consistent with  $\alpha$ - $\text{KHF}_2$  being a proton conductor and the platinum  
1847 paint electrodes behaving as reversible hydrogen electrodes. This contrasted sharply with the low  
1848 frequency behavior of  $\alpha$ - $\text{KHF}_2$  in a vacuum, where a double layer capacitance of about 440 mF  
1849  $\text{m}^{-2}$  per electrode in parallel with a Faradaic resistance of about  $2 \times 10^4 \Omega \text{m}$  per electrode

1850 produced an additional semicircle in the complex plane. For the polycrystalline  $\beta$ -phase the  
 1851 complex plane plot was essentially unchanged for data taken in both a hydrogen atmosphere and a  
 1852 vacuum [69] and is consistent with a Warburg impedance in series with a parallel RC element,  
 1853 corresponding to electrode polarization due to blocking of  $K^+$  and/or  $F^-$  charge carriers. An RC  
 1854 transmission line was used to rationalize the Warburg impedance in terms of bulk electrical  
 1855 relaxation.

#### 1856 2.4.6.5 Intergranular Effects in Polycrystalline Electrolytes

1857 The effects of intergranular material on the overall electrical response of polycrystalline  
 1858 electrolytes have been extensively documented. Only one example is discussed here [9,66]. The  
 1859 simplest equivalent circuit representation of such materials comprises two parallel RC elements  
 1860 in series, where one element is associated with a crystallite and the other with intergranular  
 1861 material. Armstrong et al. [70] showed that such a series circuit can represent the principle  
 1862 features of polycrystalline electrolytes. Since the interface is thin and the permittivities of ionic  
 1863 solids typically vary by a factor of less than 10, the capacitance  $C_i$  associated with the interface is  
 1864 much higher than that of the grain  $C_p$ :  
 1865

$$1866 \quad C_i = \frac{\epsilon_0 \epsilon' A_i}{d_i} \gg \epsilon_0 \epsilon' = k C_p \quad (2.211)$$

1868 where  $A_i$  is the average cross section area,  $d_i$  is the average thickness of the intergranular material,  
 1869 and  $k = \epsilon_0 / C_0$  is the cell constant.

#### 1871 2.4.6.6 Intergranular Cracking

1872 Experimental  $M''$  and  $\rho''$  spectra for a polycrystalline material known to have  
 1873 intergranular cracking were reported in [9]. The spectra were similar to those for two parallel  
 1874  $R_p C_p$  elements in series although the experimental peaks were broader - they could be  
 1875 approximated as the sum of two Debye peaks of equal heights separated by about a decade in  
 1876 frequency, so that the maxima in  $Z''$  and  $M''$  could be approximated as  $R_p / 4$  and  $C_0 / 4C_p$ ,  
 1877 respectively. Computed values of R and C for the intergranular and granular material in the  
 1878 cracked sample, using these approximations and assuming a resolution into symmetric  $\rho''$  peaks,  
 1879 were:  
 1880

#### 1881 Lower Frequency (Intergranular) Relaxation in Cracked Sample

$$1882 \quad \tau_i = \frac{1}{\omega_{\max(Z'')}} = 6.4 \times 10^{-6} \text{ s}, \quad (2.212)$$

$$1883 \quad R_i \approx 4Z''_{\max} = 6.4 \times 10^6 \Omega, \quad (2.213)$$

$$1884 \quad C_i = \frac{\tau_i}{R_i} \approx 1.0 \text{ pF}. \quad (2.214)$$

1886

1887 Higher frequency (Intragranular) Relaxation in Cracked Sample

$$1888 \quad \tau_c = \frac{1}{\omega_{\max}(Z'')} = 1.6 \times 10^{-7} \text{ s}, \quad (2.215)$$

$$1889 \quad R_c \approx 4Z''_{\max} = 2.6 \times 10^6 \Omega, \quad (2.216)$$

$$1890 \quad C_c = \frac{\tau_c}{R_c} \approx 0.06 \text{ pF} \quad (2.217)$$

1891  
 1892 The impedance spectrum was drastically altered after the intergranular cracking had been  
 1893 annealed out [9]. A single peak in  $Z''$  was observed in the annealed sample that was essentially  
 1894 indistinguishable from the high frequency peak in the cracked material, strongly suggesting that it  
 1895 was due to intra-crystal relaxation and that the additional low frequency peak for the cracked  
 1896 sample was due to thin air gaps. Consistent with this, the modulus spectrum was essentially  
 1897 unchanged by annealing since it was unaffected by the high capacitance cracks. The estimates of  
 1898 the intragranular and intergranular resistances were confirmed by the  $\sigma_0$  data: the observed  
 1899 conductivity of the cracked sample was largely determined by the intergranular resistance, and the  
 1900 ratio of the conductivities of the sample before and after annealing should have been

$$1902 \quad \frac{Z''_{\max}^{\text{low}\omega} + Z''_{\max}^{\text{high}\omega}}{Z''_{\max}^{\text{high}\omega}} = \frac{2.25 \times 10^6}{0.65 \times 10^6} = 3.5, \quad (2.218)$$

1903  
 1904 in fair agreement with  
 1905

$$1906 \quad \frac{\sigma_{\text{annealed}}}{\sigma_{\text{cracked}}} = 3.1. \quad (2.219)$$

1907  
 1908 The combination of modulus and impedance spectroscopies once again revealed details that could  
 1909 not be obtained from the original  $\sigma'$  and  $\varepsilon'$  data.

#### 1910 1911 2.4.6.7 Intergranular Gas Adsorption

1912 The effects of oxygen and alkali doping on the electrical response of polycrystalline zinc  
 1913 oxide were studied by Seitz and Sokoly [71]. Only the effects of oxygen pressure are discussed  
 1914 here. An increase in conductivity was observed with decreasing oxygen pressure and the absence  
 1915 of changes due to different electrode materials implied that adsorbed oxygen at grain surfaces was  
 1916 responsible for the observed polarization of the sample. The conductivity and permittivity were  
 1917 plotted explicitly as a function of frequency and these data allowed  $M''$  and  $\rho''$  spectra to be  
 1918 calculated without difficulty (unpublished results obtained by the present author). The calculated  
 1919  $M''$  and  $\rho''$  spectra exhibited two partially resolved peaks whose estimated magnitudes were  
 1920 consistent with a thin high capacitance - high resistance layer determining the low frequency  
 1921 response. Both peaks in the  $M''$  spectrum had comparable half widths (ca. 1.5 decades) and their  
 1922 relative maximum values  $8 \times 10^{-4}$  and  $1.1 \times 10^{-2}$  (ratio 14) were a good (inverse) measure of the  
 1923 relative capacitance of each relaxation:  $C_l / C_h \approx 13$ . The resistance ratio  $R_l / R_h$  of the low

1924 frequency high frequency relaxation could then be estimated from the two values of  $f_{\max}$  (ca.  
 1925  $5 \times 10^2$  and  $3 \times 10^5$  Hz) to be about 45:

1926

$$1927 \quad \frac{R_\ell C_\ell}{R_h C_h} \approx 600 \approx \frac{13R_\ell}{R_h} \Rightarrow \frac{R_\ell}{R_h} \approx 45. \quad (2.220)$$

1928

1929 The conductivity estimated from the height of the lower frequency resistivity peak was  $1.1 \times 10^{-7}$   
 1930  $\text{S m}^{-1}$ , in reasonable agreement with the low frequency plateau value of  $1.3 \times 10^{-7}$  S/m. From the  
 1931 relative frequencies of the M'' maxima and the relative heights of the (partly resolved)  $\rho''$  maxima,  
 1932 the conductivity of the high frequency relaxation was estimated to be about  $10^{-6 \pm 1}$   $\text{S m}^{-1}$ . Because  
 1933 of its higher associated capacitance the lower frequency relaxation almost certainly corresponded  
 1934 to an intergranular impedance, and its removal by a reduction in oxygen pressure should therefore  
 1935 have increased the sample conductivity by about 45 but have a small effect on the measured  
 1936 permittivity (since removal of a high series capacitance has little effect on the total impedance).  
 1937 This predicted change in resistivity agreed with the qualitative statement that conductivity  
 1938 increased with decreasing oxygen pressure [71].

1939

1940

1941 Appendices

1942

1943 Appendix 2.1 Derivation of  $M^*$  for a Debye Relaxation with No Additional Separate

1944 Conductivity

1945

These derivations are shown for pedagogical clarity rather than mathematical elegance.

1946

$$(1) \Delta\varepsilon \equiv \varepsilon_0^E - \varepsilon_\infty^E; \tau_D = (\varepsilon_\infty^E / \varepsilon_0^E) \tau_E; M_0^E = 1 / \varepsilon_0^E; M_\infty^E = 1 / \varepsilon_\infty^E$$

1947

$$(2) M^* = 1 / \varepsilon^* \Rightarrow M' = \frac{\varepsilon'}{\varepsilon'^2 + \varepsilon''^2}; M'' = \frac{-\varepsilon''}{\varepsilon'^2 + \varepsilon''^2}$$

1948

$$(3) \varepsilon' = \varepsilon_\infty^E + \frac{(\varepsilon_0^E - \varepsilon_\infty^E)}{1 + \omega^2 \tau_E^2} = \varepsilon_\infty^E + \frac{\Delta\varepsilon}{1 + \omega^2 \tau_E^2}; \varepsilon'' = \frac{\Delta\varepsilon \omega \tau_E}{1 + \omega^2 \tau_E^2}$$

$$\varepsilon'^2 + \varepsilon''^2 = (\varepsilon_\infty^E)^2 + \frac{2\varepsilon_\infty^E \Delta\varepsilon}{1 + \omega^2 \tau_E^2} + \frac{\Delta\varepsilon^2}{(1 + \omega^2 \tau_E^2)^2} + \frac{\Delta\varepsilon^2 \omega^2 \tau_E^2}{(1 + \omega^2 \tau_E^2)^2}$$

1949

$$= \frac{(\varepsilon_\infty^E)^2 (1 + \omega^2 \tau_E^2) + 2\varepsilon_\infty^E \Delta\varepsilon + \Delta\varepsilon^2}{1 + \omega^2 \tau_E^2} = \frac{(\varepsilon_0^E)^2 + (\varepsilon_\infty^E)^2 \omega^2 \tau_E^2}{1 + \omega^2 \tau_E^2}$$

$$M' = \left( \frac{\varepsilon_\infty^E (1 + \omega^2 \tau_E^2) + \Delta\varepsilon}{1 + \omega^2 \tau_E^2} \right) \left( \frac{1 + \omega^2 \tau_E^2}{(\varepsilon_0^E)^2 + (\varepsilon_\infty^E)^2 \omega^2 \tau_E^2} \right) = \left( \frac{\varepsilon_0^E + \varepsilon_\infty^E \omega^2 \tau_E^2}{(\varepsilon_0^E)^2 + (\varepsilon_\infty^E)^2 \omega^2 \tau_E^2} \right) = \left[ \frac{\varepsilon_0^E + \varepsilon_\infty^E \omega^2 \tau_E^2}{(\varepsilon_0^E)^2 \left( 1 + \frac{(\varepsilon_\infty^E)^2}{(\varepsilon_0^E)^2} \omega^2 \tau_E^2 \right)} \right]$$

1950

$$(4) = \frac{1}{\varepsilon_0^E} + \frac{\varepsilon_\infty^E \omega^2 \tau_E^2 - \frac{\varepsilon_\infty^2}{\varepsilon_0} \omega^2 \tau_E^2}{(\varepsilon_0^E)^2 \left( 1 + \frac{(\varepsilon_\infty^E)^2}{(\varepsilon_0^E)^2} \omega^2 \tau_E^2 \right)} = \frac{1}{\varepsilon_0^E} + \frac{\frac{\varepsilon_\infty^E}{(\varepsilon_0^E)^2} \omega^2 \tau_E^2 - \frac{(\varepsilon_\infty^E)^2}{(\varepsilon_0^E)^3} \omega^2 \tau_E^2}{\left( 1 + \frac{(\varepsilon_\infty^E)^2}{(\varepsilon_0^E)^2} \omega^2 \tau_E^2 \right)} = \frac{1}{\varepsilon_0^E} + \frac{\left( \frac{1}{\varepsilon_\infty^E} - \frac{1}{\varepsilon_0^E} \right) \frac{(\varepsilon_\infty^E)^2}{(\varepsilon_0^E)^2} \omega^2 \tau_E^2}{\left( 1 + \frac{(\varepsilon_\infty^E)^2}{(\varepsilon_0^E)^2} \omega^2 \tau_E^2 \right)}$$

$$= \frac{1}{\varepsilon_0^E} + \frac{\left( \frac{1}{\varepsilon_\infty^E} - \frac{1}{\varepsilon_0^E} \right) \omega^2 \tau_D^2}{(1 + \omega^2 \tau_D^2)} = M_0^E + \frac{(M_\infty^E - M_0^E) \omega^2 \tau_D^2}{(1 + \omega^2 \tau_D^2)}$$

1951

$$M'' = \left( \frac{-\Delta\varepsilon\omega\tau_E^2}{1+\omega^2\tau_E^2} \right) \left( \frac{1+\omega\tau_E^2}{(\varepsilon_0^E)^2 + (\varepsilon_\infty^E)^2 \omega^2\tau_E^2} \right) = \left( \frac{-\Delta\varepsilon\omega\tau_E}{(\varepsilon_0^E)^2 \left( 1 + \frac{(\varepsilon_\infty^E)^2}{(\varepsilon_0^E)^2} \omega^2\tau_E^2 \right)} \right)$$

1952

(5)

$$= \left( \frac{-\Delta\varepsilon \frac{1}{\varepsilon_0 \varepsilon_\infty^E} \frac{\varepsilon_\infty^E}{\varepsilon_0^E} \omega\tau_E}{\left( 1 + \frac{(\varepsilon_\infty^E)^2}{(\varepsilon_0^E)^2} \omega^2\tau_E^2 \right)} \right) = \frac{(M_\infty^E - M_0^E) \omega\tau_D}{(1 + \omega^2\tau_D^2)}$$

1953

1954

1955

1956

A Matlab®/Octave program for computing the components of  $M^*$  with added conductivity is given below in Appendix 2.2.

```

1957
1958 Appendix 2.2 Matlab®/GNU Octave Codes
1959 Computation Code for a Debye Relaxation with Additional Separate Conductivity  $\sigma_0$ .
1960 The algebraic derivation is excessively tedious and is replaced here by a
1961 Matlab®/GNU Octave code that plots both components of the  $\epsilon^*$  and  $M^*$  functions. The values
1962 of the input parameters are entered by editing the m-file.
1963
1964 % FUNCTION DebyeCondM Computes and Plots  $M^*$  for Debye  $E^*$  plus constant conductivity
1965 function HD = DebyeCondM
1966 w = logspace(-6,+6,1200);
1967 Logw = log10(w);
1968 E00 = 8.854E-12; % Vacuum permittivity in F/m
1969 E0D = 20; % Low f dielectric relative permittivity
1970 EinfD = 10; % High f dielectric relative permittivity
1971 DelE = E0D - EinfD; % Dielectric dispersion range
1972 EinfE = 3; % High f conductivity relative permittivity
1973 TauD = 10^-4 % Dielectric relaxation time
1974 Sigma0 = 10^-15; % Conductivity in S/m
1975 Tausig = E00*EinfE/Sigma0 % Conductivity relaxation time
1976 E2sig = Sigma0./(E00*w); % Conductivity contribution to E2
1977 % CALCULATE E1 and E2
1978 wTauD = w*TauD;
1979 Num = 1./(1 + wTauD.^2);
1980 E1 = EinfD + DelE*Num; % Debye E1
1981 E2 = DelE*wTauD.*Num + E2sig; % Debye E2 + Conductivity E2
1982 Denom = E1.^2 + E2.^2;
1983 M1 = E1./Denom;
1984 M2 = E2./Denom;
1985 subplot (2,2,1);
1986 plot (Logw, E1);
1987 ylabel("E1");
1988 subplot (2,2,2);
1989 plot (Logw, E2);
1990 ylabel("E2");
1991 subplot (2,2,3);
1992 plot (Logw, M1);
1993 ylabel("M1");
1994 subplot (2,2,4);
1995 plot (Logw, M2);
1996 ylabel("M2");
1997
1998 return
1999

```

2000

2001 Appendix 2.3 Derivation of Debye Dielectric Expression from Equivalent Circuit

2002 Impedance of  $R_s + C_s$  is

$$2003 \quad Z_s = R_s + 1/i\omega C_s = (1 + i\omega R_s C_s) / i\omega C_s = (1 + i\omega \tau_s) / i\omega C_s \quad (C1)$$

2004 and its admittance is

$$2005 \quad A_s = 1/Z_s = i\omega C_s / (1 + i\omega \tau_s) \quad (C2)$$

2006 where  $\tau_s \equiv R_s C_s$ . The total admittance is

$$2007 \quad A^* = i\omega C_s / (1 + i\omega \tau_s) + G_p + 1/(i\omega C_p) \quad (C3)$$

2008 and the complex capacitance is

$$C^* = A^* / i\omega = C_p + C_s / (1 + i\omega \tau_s) + G_p / i\omega$$

$$= \frac{C_p (1 + i\omega \tau_s) + C_s}{1 + i\omega \tau_s} + \frac{G_p}{i\omega} = \frac{[C_p (1 + i\omega \tau_s) + C_s] (1 - i\omega \tau_s)}{1 + \omega^2 \tau_s^2} + \frac{G_p}{i\omega}$$

$$2009 \quad = \frac{[C_p (1 + \omega^2 \tau_s^2) + C_s (1 - i\omega \tau_s)]}{1 + \omega^2 \tau_s^2} - \frac{iG_p}{\omega} \quad (C4)$$

$$= \frac{[C_p (1 + \omega^2 \tau_s^2) + C_s]}{1 + \omega^2 \tau_s^2} - \frac{i\omega \tau_s C_s}{1 + \omega^2 \tau_s^2} - \frac{iG_p}{\omega}$$

2010 from which eqs. (2.157) and (2.158) obtain.

2011

2012

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